



Course File Check List

- ✓1. Contents
 - * 2. Academic calendar of VTU, Institute and Department
 - ✓3. Vision, Mission statements of Institute
 - ✓4. Vision, Mission, PEOs, POs, PSOs statements of Department
 - ✓5. Individual time table
 - ✓6. Syllabus
 - ✓7. Course Articulation Matrix [CO-PO, CO-PSO mapping]
 - ✓8. Lesson plan
 - ✓9. Text books / Reference books referred
 - ✓10. Attendance register
 - ✓11. Course material
 - ✓a) Notes
 - b) PPT
 - c) NPTEL / Youtube Videos
 - 12. Additional topics taken to meet the POs.
 - a) Site visits
 - b) Technical talks
 - c) Quiz
 - d) Group discussion
 - e) Blended learning
 - f) Model making competition
 - g) Modern tool (Computing tool) usage
 - ✓13. Exam question papers
 - ✓14. Test and Assignment question papers (with scheme of evaluation)
 - ✓15. Result analysis
 - * a) Percentage CO covered / Percentage of CO addressed.
 - * b) CO-PO and CO-PSO Attainment
 - * c) Percentage of students passed
 - 16. Counselling report (Actions taken to improve Weak students / Slow learners)
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Wapuji Institute of Engineering and Technology, Duvangare-577004
CALENDAR OF EVENTS - ODD SEMESTER: SEPTEMBER-JANUARY-2020-21 (Tentative)

PARTICULARS	I sem	III, V	VI sem	VI & V sem	III sem	III sem
1 st SEM Computer course of ODD Sem Class Work and Ex	REAR Tech 1-12-2020 28-03-2021	REAR Tech 01-09-2020 16-01-2021 19-10-2020 To	REAR Tech 01-09-2020 16-01-2021 19-10-2020 To	MCA 01-09-2020 16-01-2021 19-10-2020 To	MBA 01-09-2020 16-01-2021 15-10-2020 To	M.Tech 01-09-2020 16-01-2021 19-10-2020 To
2 nd SEM		To 24-10-2020 07-12-2020 To	To 24-10-2020 07-12-2020 To	To 24-10-2020 07-12-2020 To	To 17-12-2020 26-11-2020 To	To 24-10-2020 07-12-2020 To
3 rd SEM		To 09-12-2020 11-01-2021 To	To 09-12-2020 11-01-2021 To	To 09-12-2020 11-01-2021 To	To 28-11-2020 7-01-2021 To	To 09-12-2020 11-01-2021 To
4 th SEM		To 13-01-2021 21-01-2021 Onwards #	To 13-01-2021 21-01-2021 Onwards #	To 13-01-2021 08-02-2021 Onwards #	To 9-01-2021 ---	To 13-01-2021 21-01-2021 Onwards #
Practical Examination	29-05-2021 12-04-2021 To	Onwards # 08-02-2021 To	Onwards # 08-02-2021 To	Onwards # 21-01-2021 To	21-01-2021 To	28-01-2021 To
Theory Examination	30-04-2021 To	27-03-2021 To	27-03-2021 29-03-2021 To	06-02-2021 To	19-02-2021 To	13-02-2021 To
Internship						
Internship Viva-Voce						
Professional Training/ Organization Study						
Conductment of Extra Semester Examination regarding the calendar of events relating to the conduct of University Examination will be issued by the	03-05-2021	29-03-2021	12-04-2021	15-02-2021	05-04-2021	23-02-2021

to facilitate (Evaluation) from time to time.

Principal



Vision of BIET

To be a center of excellence recognized nationally and internationally, in distinctive areas of engineering education and research, based on a culture of innovation and invention.

Mission of BIET

BIET contributes to the growth and development of its students by imparting a broad based engineering education and empowering them to be successful in their chosen field by inculcating in them positive approach, leadership qualities and ethical values



VISION OF THE DEPARTMENT

To train the students to become Civil Engineers with leadership qualities, having ability to take up professional assignments and research with a focus on innovative approaches to cater to the needs of the society.

MISSION OF THE DEPARTMENT

1. To provide quality education through updated curriculum and conducive teaching learning environment for the students to excel in higher studies, competitive examinations and professional career.
2. To impart soft skills, leadership qualities and professional ethics among the graduates to handle the projects independently with confidence.
3. To deal with the contemporary issues and to cater to the socio-economic needs.
4. To build industry-institute interaction and to establish good rapport with alumni.

PROGRAM EDUCATIONAL OBJECTIVES (PEOs)

PEO 1: Core Competence: Graduates will be able to plan, analyse, design and construct sustainable Civil Engineering Infrastructure.

PEO 2: Professional Skills: Graduates will be professional engineers with a sense of ethics, creativity, leadership, self-confidence and independent thinking to cater to the needs of the society.

PEO 3: Societal Needs: Graduates will be able to contribute effectively for the development of industry and professional bodies.

PEO 4: Cognitive Intelligence: Graduates will be able to take up competitive examinations, higher studies and involve in research and entrepreneurship activities.

PROGRAM SPECIFIC OUTCOMES (PSOs)

Students after the completion of the Program will be able to

1. Apply the fundamental concepts, software and codal provisions in the analysis, design and construction of sustainable civil engineering infrastructure.
2. Inculcate professional and leadership qualities, sense of ethics and confidence related to civil engineering.

Faculty will be able to

3. Contribute to the overall development of civil engineering community through the professional bodies and offer services to the society.
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Name of the Faculty : Sri. Sharathraj R M

Time / Day	8 – 9	9 – 10	10.30 – 11.30	11.30 – 12.30	2 – 3	3 – 4	4 – 5
Mon	17CV53 – PS			18CV33 – A			
Tue	18CV33 – A			17CV53 – PS	18CVL57 – A2 (SRM + CTG)		
Wed							
Thu		17CV53 – PS					
Fri		17CV53 – PS			18CVL57 – B2 (SRM + VMK)		
Sat		18CVL37 – B3 (SH + SRM)	18CV33 – A				

Time Table Coordinator

HOD

Principal

F141

B. E. CIVIL ENGINEERING			
Choice Based Credit System (CBCS) and Outcome Based Education (OBE)			
SEMESTER - III			
FLUIDS MECHANICS			
Course Code	18CV33	CIE Marks	40
Teaching Hours/Week(L:T:P)	(3:0:0)	SEE Marks	60
Credits	03	Exam Hours	03
<p>Course Learning Objectives: The objectives of this course is to make students to learn:</p> <ol style="list-style-type: none"> 1. The Fundamental properties of fluids and its applications. 2. Hydrostatic laws and application to solve practical problem. 3. Principles of Kinematics and Hydrodynamics for practical applications. 4. Basic design of pipes and pipe networks considering flow, pressure and its losses. 5. The basic flow rate measurements. 			
Module-1			
<p>Fluids & Their Properties: Concept of fluid, Systems of units. Properties of fluid; Mass density, Specific weight, Specific gravity, Specific volume, Viscosity, Newton's law of viscosity (theory & problems), Cohesion, Adhesion, Surface tension, Pressure inside a water droplet, soap bubble and liquid jet. Numerical problems, & Capillarity. Capillary rise in a vertical tube and between two plane surfaces (theory & problems). Vapor pressure of liquid, compressibility and bulk modulus, Fluid as a continuum,</p> <p>Fluid Pressure and Its Measurements: Definition of pressure, Pressure at a point, Pascal's law, Variation of pressure with depth. Types of pressure. Measurement of pressure using simple, differential & inclined manometers (theory & problems). Introduction to Mechanical and electronic pressure measuring devices.</p>			
Module-2			
<p>Hydrostatic forces on Surfaces: Definition, Total pressure, centre of pressure, total pressure on horizontal, vertical and inclined plane surface, total pressure on curved surfaces, water pressure on gravity dams, Lock gates. Numerical Problems.</p> <p>Fundamentals of fluid flow (Kinematics): Introduction. Methods of describing fluid motion. Velocity and Total acceleration of a fluid particle. Types of fluid flow, Description of flow pattern. Basic principles of fluid flow, three- dimensional continuity equation in Cartesian coordinate system. <u>Derivation</u> for Rotational and irrotational motion. Potential function, stream function, orthogonality of streamlines and equipotential lines. Numerical problems on Stream function and velocity potential. Introduction to flow net.</p>			
Module-3			
<p>Fluid Dynamics: Introduction. Forces acting on fluid in motion. Euler's equation of motion along a streamline and Bernoulli's equation. Assumptions and limitations of Bernoulli's equation. Modified Bernoulli's equation. Problems on applications of Bernoulli's equation (with and without losses). Momentum equation problems on pipe bends.</p> <p>Applications: Introduction. Venturi meter, Orifice meter, Pitot tube. Numerical Problems.</p>			
Module-4			
<p>Orifice and Mouth piece: Introduction, classification, flow through orifice, hydraulic coefficients and Numerical problems. Mouthpiece, classification, Borda's Mouthpiece (No problems).</p> <p>Notches and Weirs: Introduction. Classification, discharge over rectangular, triangular, trapezoidal notches, Cippoletti notch, broad crested weirs. <u>Numerical problems.</u> Ventilation of weirs, submerged weirs,</p>			
Module-5			

Flow through Pipes: Introduction. Major and minor losses in pipe flow. Darcy- Weis bach equation for head loss due to friction in a pipe. Pipes in series, pipes in parallel, equivalent pipe-problems. Minor losses in pipe flow, equation for head loss due to sudden expansion. Numerical problems. Hydraulic gradient line, energy gradient line. Numerical problems, .Pipe Networks, Hardy Cross method (No problems on pipe networks),

Surge Analysis in Pipes: Water hammer in pipes, equations for pressure rise due to gradual valve closure and sudden closure for rigid and elastic pipes. Problems.

Course outcomes: After successful completion of the course, the student will be able to:

1. Possess a sound knowledge of fundamental properties of fluids and fluid Continuum
2. Compute and solve problems on hydrostatics, including practical applications
3. Apply principles of mathematics to represent kinematic concepts related to fluid flow
4. Apply fundamental laws of fluid mechanics and the Bernoulli's principle for practical applications
5. Compute the discharge through pipes and over notches and weirs

Question paper pattern:

- The question paper will have ten full questions carrying equal marks.
- Each full question will be for 20 marks.
- There will be two full questions (with a maximum of four sub- questions) from each module.
- Each full question will have sub- question covering all the topics under a module.
- The students will have to answer five full questions, selecting one full question from each module.

Textbooks:

1. P N Modi and S M Seth, "Hydraulics and Fluid Mechanics, including Hydraulic Machines", 20th edition, 2015, Standard Book House, New Delhi
2. R.K. Bansal, "A Text book of Fluid Mechanics and Hydraulic Machines", Laxmi Publications, New Delhi
3. S K SOM and G Biswas, "Introduction to Fluid Mechanics and Fluid Machines", Tata McGraw Hill, New Delhi

Reference Books:

1. Victor L Streeter, Benjamin Wylie E and Keith W Bedford, "Fluid Mechanics", Tata McGraw Hill Publishing Co Ltd., New Delhi, 2008(Ed).
2. K Subramanya, "Fluid Mechanics and Hydraulic Machines", Tata McGraw Hill Publishing Co. Ltd.
3. K Subramanya, "Fluid Mechanics and Hydraulic Machines-problems and solutions", Tata McGraw Hill Publishing Co. Ltd.
4. J. F. Douglas, J. M. Gasoriek, John Swaffield, Lynne Jack, "Fluid Mechanics", Pearson, Fifth Edition.
5. Mohd. Kaleem Khan, "Fluid Mechanics and Machinery", Oxford University Press.

Course Title	Fluid Mechanics (18CV33)
CO	Statement
18CV33.1	Explain the fundamental properties of fluids
18CV33.2	Explain the concept of fluid pressure and equipment for its measurement
18CV33.3	Calculate the hydrostatic forces acting on surfaces and explain the kinematic concepts of fluid flow
18CV33.4	Apply Euler's equation and Bernoulli's principle for the practical applications of fluid flow
18CV33.5	Compute the discharge through channels and pipes
18CV33.6	Explain the losses in pipe flow and effect of water hammer in pipe flow

Course Title		Fluid Mechanics										
CO	PO1	PO2	PO3	PO4	PO5	PO6	PO7	PO8	PO9	PO10	PO11	PO12
18CV33.1	2	2	-	1	-	-	-	-	-	-	-	2
15CV33.2	2	2	-	1	-	-	-	-	-	-	-	2
15CV33.3	2	2	-	1	-	-	-	-	-	-	-	2
15CV33.4	2	2	-	1	-	-	-	-	-	-	-	2
15CV33.5	2	2	-	1	-	-	-	-	-	-	-	2
15CV33.6	2	2	-	1	-	-	-	-	-	-	-	2
Average	2	2		1								2

CO	PSO1	PSO2
18CV33.1	2	2
15CV33.2	2	2
15CV33.3	2	2
15CV33.4	2	2
15CV33.5	2	2
15CV33.6	2	2
Average	2	2

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. 32. 33. 34. 35. 36. 37. 38. 39. 40. 41. 42. 43. 44. 45. 46. 47. 48. 49. 50. 51. 52. 53. 54. 55. 56. 57. 58. 59. 60. 61. 62. 63. 64. 65. 66. 67. 68. 69. 70. 71. 72. 73. 74. 75. 76. 77. 78. 79. 80. 81. 82. 83. 84. 85. 86. 87. 88. 89. 90. 91. 92. 93. 94. 95. 96. 97. 98. 99. 100.

LESSON PLAN

Subject: FLUID MECHANICS Subject Code: 18CV33

Class: III.A. CV

| Period | Date | Topics Planned | Date | Topics Covered | Remarks |
|--------|------------|--|------------|---|---------|
| 1 | 1/9/2020 | <u>Module - 1</u>
Concept of fluid.
System of units
Properties of fluid | 6/10/20 | Concept of fluid.
System of units
properties of fluid. | |
| 2 | 5/9 | Mass density, Sp weight
Sp. gravity, Sp. Volume
viscosity, Newtons law of
viscosity | 7/10/20 | Mass density, Specific
weight, specific gravity
viscosity | |
| 3 | 7/9 | Cohesion, Adhesion
Surface tension
pressure inside a water
droplet | 8/10/20 | cohesion, Adhesion
surface tension
pressure inside ^{water} droplet | |
| 4 | 8/9 | Soap bubble, liquid jet
capillarity, capillary
rise in a vertical tube. | 13/10/20 | Soap bubble, liquid
jet, capillarity rise
in a vertical tube. | |
| 5 | 12/9 | Vapour pressure of
liquid, compressibility
and bulk modulus. | 14/10 | Vapour pressure of
liquid, compressibility
and bulk modulus | |
| 6 | 14/9 | Pressure, Pascals law
Variation of pressure
with depth, types of pressure | 15/10 | problems | |
| 7 | 15/9 | Measurement using
Simple, differential
and Inclined Manometer | 20/10 | pressure & its
measurements | |
| 8 | 19/9 | Mechanical and
Electrical pressure
measuring devices. | 22/10 | problems. | |
| 9 | 21/9/2020 | <u>Module - 2</u>
Total pressure, Centre of
pressure, TP on Horizontal
surface. | 7/11/2020 | Module 1-2
total pressure &
centre of pressure. | |
| 10 | 22/9 | Vertical and Inclined
surface, total pressure
on curved surfaces. | 9/11/2020 | Horizontal, Vertical
Inclined, curved
surfaces | |
| 11 | 26/9 | Water pressure on
gravity dams, Lockgates
Methods of fluid motion | 10/11/2020 | Water pressure on
gravity dams, lockgates
methods of fluid motion. | |
| 12 | 23/9/2020 | Velocity and total acc ⁿ
of a fluid particle.
Type of fluid flow, flow
pattern | 12/11 | velocity & total
acceleration of fluid
particle, type of flow | |
| 13 | 29/9 | Basic principles of fluid
flow 3 Dimensional continuity
equation in Cartesian co-system | 17/11 | Basic principles of
fluid flow in 3D
continuity equation. | |
| 14 | 03/10/2020 | Derivation for Rotational
and Irrotational motion
Potential function. | 21/11 | Derivation for rotation
and irrotational
motion, potential function. | |
| 15 | 5/10 | Stream function,
Orthogonality of streamlines | 23/11 | Stream function,
orthogonality of | |

LESSON PLAN

Subject: Fluid Mechanics Subject Code: 18 CV 33

Class: III. A. CV

| Period | Date | Topics Planned | Date | Topics Covered | Remarks |
|--------|-----------|--|----------|---|---------|
| 18 | 12/10 | Bernoulli's equation, Assumpt and limitations. Modified Bernoulli equation. | 30/11 | Bernoulli equation, Assumptions, Limitation modified Bernoulli eq | |
| 19 | 13/10 | problems on application of Bernoulli's eq ⁿ with losses | 01/12/20 | problems | |
| 20 | 17/10 | problems on application of Bernoulli's eq ⁿ without losses. | 05/12 | problems | |
| 21 | 19/10 | Momentum equation problems on pipe bends | 08/12 | momentum equation problems. | |
| 22 | 20/10 | Applications: Introduction, Venturimeter | 12/12 | Applications of Bernoulli's equation venturimeter. | |
| 23 | 24/10 | Orifice meter, pitot tube, problems | 14/12 | problems on Venturimeter. | |
| 24 | 27/10 | problems. | 15/12 | problems. | |
| 25 | 2/11/2020 | Module - 4. Orifice and mouthpiece classification, flow through orifice | 19/12 | Module - 4. orifice and mouthpiece, classification, | |
| 26 | 3/11 | Hydraulic coefficient. problems. | 21/12 | Hydraulic coefficient Cd, Cv, Ce, Cr. | |
| 27 | 7/11 | Mouthpiece, classification Borda's mouthpiece | 22/12 | Mouthpieces, types Borda's mouthpiece, | |
| 28 | 9/11 | Notches & Weirs: types discharge over Rectangular notches. | 26/12 | Notches & weirs, types, | |
| 29 | 10/11 | triangular, trapezoidal Cipolletti notch. | 28/12 | Derivation of Q over Rectangular, triangular trapezoidal notch | |
| 30 | 17/11 | broad crested weirs problems. | 29/12 | Broad crested weirs problems. | |
| 31 | 21/11 | problems. | 02/01/21 | problems. | |
| 32 | 23/11 | Ventilation of weirs, Submerged weirs. | 05/01 | ventilation of weirs submerged weirs | |
| 33 | 24/11 | Module 5. Flow through pipes. Introduction, major & minor losses in pipe flow. Darcy-Weisbach equation | 09/01 | Module 5. Flow through pipes. losses in pipe flow | |

Text Books :

1. P. N. Modi and S. M. Seth, "Hydraulics & Fluid mechanics including hydraulic machines", 20th Edition
2. R. K. Bansal "Fluid Mechanics and Hydraulic Machines" Laxmi publications.

Reference Books :

1. Victor L. Stretter, Benjamin Wylie F and Keith "Fluid Mechanics" Tata McGraw publishing co. Ltd.
2. K. Subramanya "Fluid Mechanics and Hydraulic Machines" Tata McGraw Hill publishing Co. Ltd.
3. K. Subramanya "Fluid Mechanics & Hydraulic Machines problems and solutions" Tata M.C. Graw Hill Publ.
4. J. P. Douglas, J. M. Gasarik, John Swaffield, Lynn Jack "Fluid Mechanics" Pearson. 5th edition
5. Mohd. Kaleem Khan "Fluid Mechanics and Machinery" Oxford university press.

Class: III . A . CV

Subject Code: ISCV33

Subject: FLUID MECHANICS

Total No. of Classes: 4

| Sl No. | USN | NAME | DATE | Subject Code: ISCV33 | | | | | | | | | | Average | Remarks | | | | | | | | | | | | | | |
|--------|-------------|------------------------|------|----------------------|---|---|---|---|---|---|---|---|----|---------|---------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | | | | | | | | | | | | | | | |
| 31 | ABD19CV061 | Shreya D K | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 32 | ABD19CV063 | Soundarya N M | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 33 | ABD19CV065 | Suathi V Kote | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 34 | ABD19CV067 | U . Madhusree | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 35 | ABD19CV069 | Vaishnavi V | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 36 | ABD19CV071 | Veeresh K X | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 37 | ABD19CV073 | Vijayalakshmi R Telkar | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 38 | ABD19CV075 | Vikas S.M. | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 39 | ABD19CV077 | Vivekananda H M | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 40 | ABD19CV079 | Yug B Jain | | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | |
| 41 | ABD18CV099 | Vinay Kumar M | | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | |
| 42 | ABD17CV052 | Mohammed Aghar Basith | | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | |
| 43 | ABD20CV413 | Touptthi S.R | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 44 | ABD18CV027 | Hareshri N | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 45 | ABD20CV406 | Channesh H Patil | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 46 | ABD18CV076 | Shivaraj K.H | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 47 | ABD20CV404 | Bharath seddy N | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 48 | ABD20CV423 | Mohammed Khadir | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 49 | ABD20CV400 | Abhilash S.V | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 50 | ABD20CV412 | Dhanush . R | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 51 | ABD20CV439 | Surabhi S Bharadwaj | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | |
| 52 | ABD20CV407 | Chelan Kobraiah. | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 53 | ABD20CV448 | Nimod Kumar Budhihal | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 54 | ABD20CV429 | Nandesh m. mathad | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 55 | ABD19CV082 | Sankhesh S Bageer | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 56 | left course | Sujith R | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 57 | ABD20CV431 | Rehith A | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 58 | ABD19CV081 | Kiran M.M. | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 59 | ABD20CV440 | Surej N Raikar | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 60 | ABD20CV428 | Munughaaendora HV | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 61 | ABD20CV422 | Charee Shaha T.R | | A | A | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |

| Class : 3A | | Subject Code : 18CV33 | | Subject : Fluid Mechanics | | Total No. of Classes : 14 | |
|------------|-----|-----------------------|------|---------------------------|----------|---------------------------|----------|
| SI No. | USN | NAME | DATE | 18/10/21 | 19/10/21 | 20/10/21 | 21/10/21 |
| | | | | 18/11/21 | 19/11/21 | 20/11/21 | 21/11/21 |
| | | | | 18/12/21 | 19/12/21 | 20/12/21 | 21/12/21 |
| | | | | 18/01/22 | 19/01/22 | 20/01/22 | 21/01/22 |
| | | | | 18/02/22 | 19/02/22 | 20/02/22 | 21/02/22 |
| | | | | 18/03/22 | 19/03/22 | 20/03/22 | 21/03/22 |
| | | | | 18/04/22 | 19/04/22 | 20/04/22 | 21/04/22 |
| | | | | 18/05/22 | 19/05/22 | 20/05/22 | 21/05/22 |
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FLUID AND THEIR PROPERTIES

MI (a)

"Fluid Mechanics" is the branch of science which deals with behaviour of fluids at rest as well as in motion.

The study of fluids in motion where pressure force are not considered is called "fluid kinematics" and if force pressure considered it is called "fluid dynamics."

Properties of fluids:

Certain characteristics of a continuous fluid are independent of the motion of a fluid. These characteristics are called basic properties of the fluid.

(1) Density or Mass density or Specific mass (ρ)

It is defined as the ratio of the mass of a fluid to its volume or Mass per unit volume of fluid unit is kg/m^3 . Mass density of water is 1000 kg/m^3 . Density of liquid is constant where as the gases changes with pressure and temperature.

$$\rho = \frac{\text{mass of fluid}}{\text{Volume of fluid}} = \frac{m}{V}$$

(2) Specific weight or weight density (w):

Defined as the ratio between the weight of a fluid to its volume.

$$w = \frac{\text{weight of fluid}}{\text{Volume of fluid}} \quad (1)$$

$$w = \frac{(\text{mass of fluid}) \times (\text{Acceleration due to gravity})}{\text{Volume of fluid}} \quad (2)$$

$$w = \frac{m \times g}{V}$$

$$w = \rho g$$

Unit is N/m^3

Volume of specific weight of water
is (1000×9.81) i.e. $(\rho \times g)$
 $= 9810 \text{ N/m}^3$

(3) Specific volume:

It is defined as the volume occupied by the unit mass or volume per unit mass of fluid. It is expressed as

$$\text{Specific volume} = \frac{\text{Volume of fluid}}{\text{mass of fluid}} \text{ or } \frac{\text{Vol. of fluid}}{\text{weight of fluid}}$$

$$= \frac{1}{\frac{\text{mass of fluid}}{\text{Volume of fluid}}}$$

$$= \frac{1}{\rho} = \frac{1}{\text{mass density}}$$

Unit is m^3/kg

(4) Specific gravity:

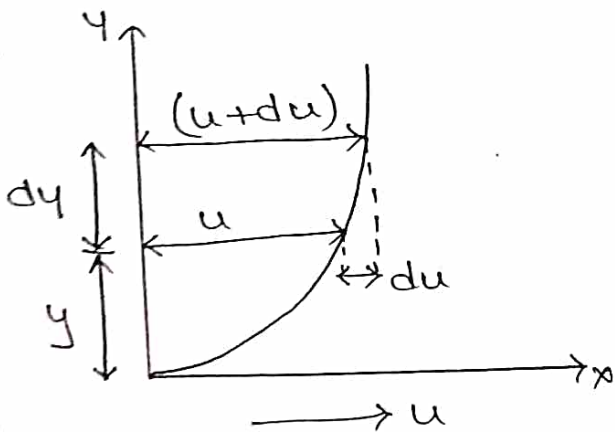
Specific gravity is defined as, ratio of weight density (or density) of fluid to the weight density (or density) of a standard fluid.

$$S = \frac{\text{Specific weight of fluid}}{\text{Specific weight of standard fluid}}$$
$$= \frac{\text{mass density of fluid}}{\text{mass density of standard fluid.}}$$

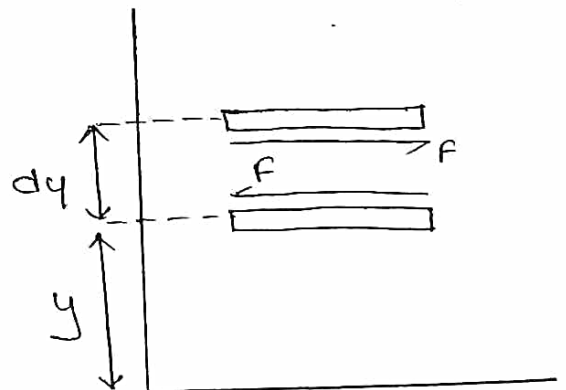
Specific gravity of water at standard temperature is 1.

(5) Viscosity:

Viscosity is defined as, property of fluid which offers resistance to the movement of one layer of fluid over another adjacent layer of fluid.



fig(c) velocity profile of parallel flow of fluid



fig(d) Two adjacent layers of moving fluid.

Consider a flow in which all fluid particles are moving in the same direction in such a way that fluid layers move parallel with different velocities. Fig (d) represents adjacent layers of fluid at a distance y from reference axis. When a distance of dy apart layers of liquid at a distance of dy apart moving one over the other at different velocities, the top layer causes shear stress on adjacent lower layer, while the lower layer causes shear stress on adjacent top layer. Shear stress is proportional to rate of change of velocity with respect to y .

Mathematically, $\tau \propto \frac{du}{dy}$

$$\tau = \mu \frac{du}{dy} \longrightarrow \textcircled{1}$$

where, μ = coefficient of dynamic viscosity
 $\frac{du}{dy}$ = rate of change of shear strain or velocity gradient.

From $\textcircled{1}$, we have $\mu = \frac{\tau}{du/dy} \longrightarrow \textcircled{2}$

[Thus viscosity is also defined as shear stress required to produce unit rate of shear strain.]

[unit is Ns/m^2]

Kinematic viscosity (ν)

It is defined as the ratio of dynamic viscosity to density of fluid.

$$\nu = \frac{\text{dynamic viscosity}}{\text{mass density}} = \frac{\mu}{\rho}$$

Unit is m^2/s

Newton's law of Viscosity

It states that shear stress τ on a fluid element layer is directly proportional to the rate of shear strain.

$$\tau \propto \frac{du}{dy}$$

$$\tau = \mu \times \frac{du}{dy}$$

Variation of viscosity with temperature

Temperature affects the viscosity. The viscosity of liquid decreases with the increase of temperature while the viscosity of gases increases with increase of temperature. This is due to the reason that the viscous forces of a fluid are due to cohesive forces and molecular momentum transfer.

In liquids the cohesive forces predominate the molecular momentum transfer due to closely packed molecules and with the increase in temperature cohesive forces decrease with the result of decreasing

viscosity. But in cases of gases, the cohesive forces are small and molecular momentum transfer predominates, with increase in temperature, molecular momentum transfer increases and hence viscosity increases.

The relation between viscosity and temperature for liquids and gases are:

(i) For liquids, $\mu = \mu_0 \left(\frac{1}{1 + \alpha t + \beta t^2} \right) \longrightarrow \textcircled{1}$

where, μ = viscosity of liquid at $t^\circ\text{C}$ in poise
 μ_0 = viscosity of liquid at 0°C in poise
 α and β are constants.

For water $\mu_0 = 1.79 \times 10^{-3}$ poise, $\alpha = 0.03368$
 and $\beta = 0.00021$

Thus eq. (1) shows that with increase of temperature the viscosity decreases.

(ii) For gas,

$$\mu = \mu_0 + \alpha t - \beta t^2 \longrightarrow \textcircled{2}$$

where for air $\mu_0 = 0.000017$, $\alpha = 0.00000005$
 $\beta = 0.1189 \times 10^{-9}$, eq. (2) shows that with increase of temperature viscosity increases.

① Hydrostatic Pressure on Surfaces:

Total Pressure force:

It is defined as the force exerted by static fluid on a surface (either plane or curved) when the fluid comes in contact with the surface. This force is always at right angles (or normal) to the surfaces.

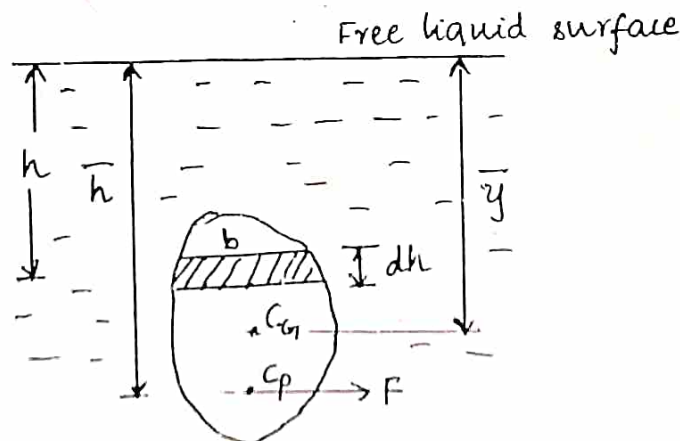
Centre of Pressure:

It is defined as the point of application of the total pressure on the surface. There are four cases of submerged surfaces on which the total pressure force and centre of pressure is to be determined.

The submerged surfaces may be :

1. Vertical plane surface
2. Horizontal plane surface
3. Inclined plane surface
4. Curved surface.

Vertical plane surface submerged in liquid:



consider a plane vertical surface of arbitrary shape immersed in a static mass of liquid. of specific

weight w as shown in fig. Let 'A' be the total area of surface.

C_G - centroid of plane surface

\bar{y} - Distance of C_G of area from free surface of liquid

F - Total pressure force

C_p - centre of pressure

\bar{h} - Distance of C_p from free surface of liquid

consider a strip of thickness dh and width b at a depth of h from free surface of liquid as shown in the figure.

Pressure intensity ~~at~~ ^{on} strip $P = wh$

Area of strip, $dA = b \cdot dh$

Then pressure force on elemental strip

$$\begin{aligned} \text{i.e. } dF &= p \times dA \\ &= wh \times dA \end{aligned}$$

\therefore Total pressure on the whole surface

$$F = \int dF = \int wh \cdot dA$$

$$F = w \int h dA$$

From basic principle of mechanics,

$$\int h dA = A \bar{y}$$

\therefore Total pressure force $\boxed{F = WA \bar{y}}$

To find the position of total pressure i.e. centre of pressure,

Centre of pressure is calculated by using principle of moments which states that moments of the resultant force about an axis is equal to sum of moments of its components about the same axis.

Moment of force F about the surface of liquid is equal to $= F \times \bar{h} \longrightarrow \textcircled{1}$

Moment of force dF acting on the strip about the free liquid surface $= dF \times h$
 $= wh \cdot b \cdot dh \cdot h.$
 $= wh^2 b dh.$

Sum of moments of all such forces about free surface of liquid $= \int wh^2 b dh.$ $dA = b \cdot dh$

$$= W \int h^2 dA$$

But $\int h^2 dA =$ moment of inertia of the surface about free liquid surface

$$\int h^2 dA = I_0$$

$$= WI_0 \longrightarrow \textcircled{2}$$

Equating $\textcircled{1}$ and $\textcircled{2}$

$$F \times \bar{h} = WI_0$$

$$\bar{h} = \frac{WI_0}{F}$$

$$\bar{h} = \frac{W I_0}{W A \bar{y}}$$

$$\boxed{\bar{h} = \frac{I_0}{A \bar{y}}}$$

$$\boxed{\bar{h} = \frac{I_G}{A \bar{y}} + \bar{y}}$$

We know $F = W A \bar{y}$

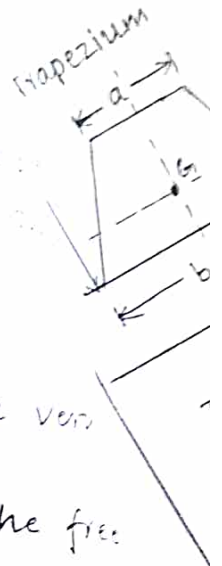
By parallel axis theorem

$$I_0 = I_G + A(\bar{y})^2$$

$$\frac{I_G + A \bar{y}^2}{A \bar{y}}$$

$\textcircled{3}$

I_G - Moment of inertia of area about an axis through C_G of area and parallel to the free surface of liquid



From the above equation it is clear that,

- (1) centre of pressure \bar{h} lies below $C.G$ of the vertical surface
- (2) The distance of the centre of pressure from the free surface of liquid is independent of the density of the liquid.

Moment of Inertia & other geometric properties of some important plane surfaces.

| Plane Surface | C_G from the base | Area | Moment of inertia about an axis passing through C_G and parallel to base (I_G) | Moment of inertia about base (I_0) |
|------------------|---------------------|---------------------|--|--|
| 1. Rectangle
 | $x = d/2$ | bd | $\frac{bd^3}{12}$ | $\frac{bd^3}{3}$ |
| 2. Triangle
 | $x = h/3$ | $\frac{bh}{2}$ | $\frac{bh^3}{36}$ | $\frac{bh^3}{12}$ |
| 3. Circle
 | $x = d/2$ | $\frac{\pi d^2}{4}$ | $\frac{\pi d^4}{64}$ | - |

h' - distance of C_p from O-O

Consider a small strip of area dA at a depth, the free liquid surface and at a distance h from as shown in fig.

i) To find the total pressure (F)

Pressure intensity on strip $p = wxh$

$$\begin{aligned} \text{Pressure force on the strip } dF &= p \times dA \\ &= wxh \times dA \end{aligned}$$

Total pressure on the whole area,

$$F = \int dF = w \int h dA$$

$$\text{From fig, } \frac{h}{h'} = \frac{\bar{y}}{\bar{y}'} = \frac{h}{h'} = \sin \theta$$

$$h = h' \sin \theta$$

$$F = w \int h' \sin \theta dA$$

$$= w \sin \theta \int h' dA$$

$$\text{we know } \int h' dA = A \bar{y}'$$

$$F = w \sin \theta A \bar{y}'$$

$$F = WA \bar{y}' \sin \theta$$

$$F = WA \bar{y}$$

$$\text{we know, } \bar{y}' \sin \theta = \bar{y}$$

Note: Therefore for a plane surface is submerged in a static mass of liquid held vertical or inclined,

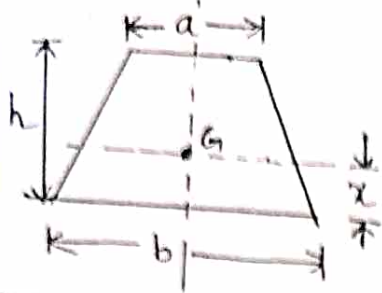
Total pressure = Product of pressure intensity at the centroid of area and the area of the plane surface.

(ii) To find centre of pressure (h_c)

$$\text{Pressure force on the strip } dF = wh dA$$

$$= wh' \sin \theta dA$$

4. Trapezium



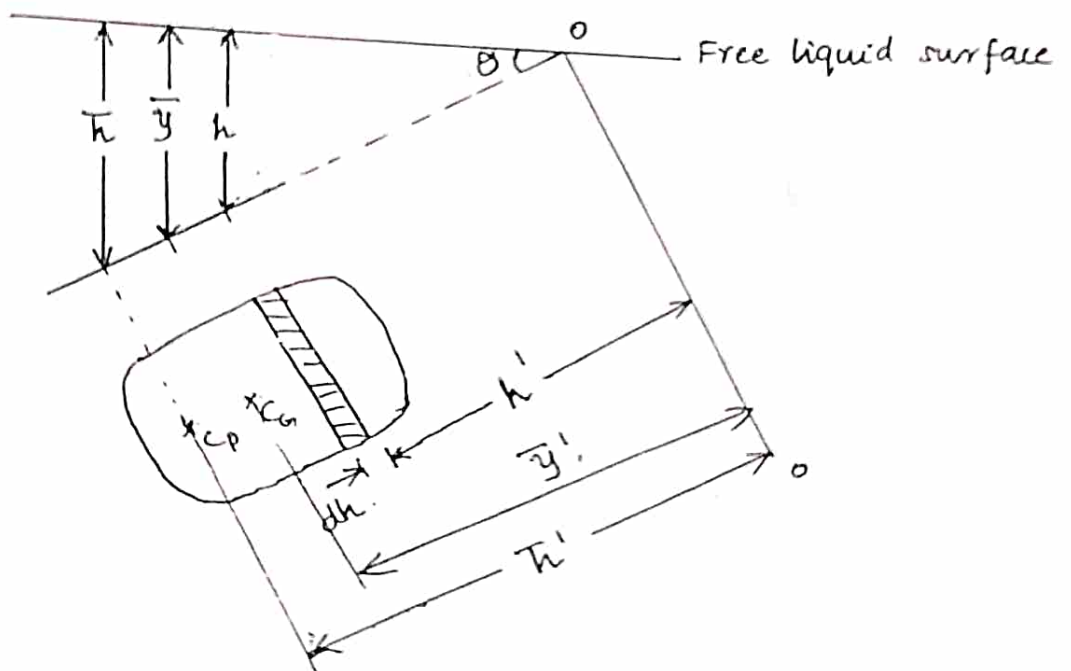
$x =$

$$\frac{(2a+b)h}{3}$$

$$\left(\frac{a+b}{2}\right) \times h$$

$$\frac{(a^2 + 4ab + b^2)}{3b(a+b)} \times h^3$$

Inclined Plane surface submerged in liquid :



Consider a plane surface of arbitrary shape immersed in a static mass of liquid of specific weight 'w' in such a way that the plane of surface makes angle θ with the free surface of liquid as shown in fig. Let A - total area of inclined surface

\bar{y} - depth of C_G of area from free liquid surface

\bar{h} - Distance of centre of pressure from free liquid surface

Let \bar{y}' = Distance of C_G of the \sin inclined surface from o.o.

(1) Dynamics of fluid flow is the study of fluid motion with the forces causing flow. The dynamic behaviour of the fluid flow is analysed by the Newton's second law of motion, which relates the acceleration with the forces. The fluid is assumed to be incompressible and non viscous.

Equations of Motion:

According to Newton's second law of motion, the net force F_x acting on a fluid element in the direction of x is equal to mass m of the fluid element multiplied by the acceleration a_x , in the x direction.

Thus mathematically,

$$F_x = m \cdot a_x \longrightarrow \textcircled{1}$$

In the fluid flow, following forces are present.

- (i) F_g , Gravity force
- (ii) F_p , Pressure force
- (iii) F_v , Force due to viscosity
- (iv) F_t , Force due to turbulence
- (v) F_c , Force due to compressibility

Thus eqⁿ $\textcircled{1}$, the net force,

$$F_x = (F_g)_x + (F_p)_x + (F_v)_x + (F_t)_x + (F_c)_x$$

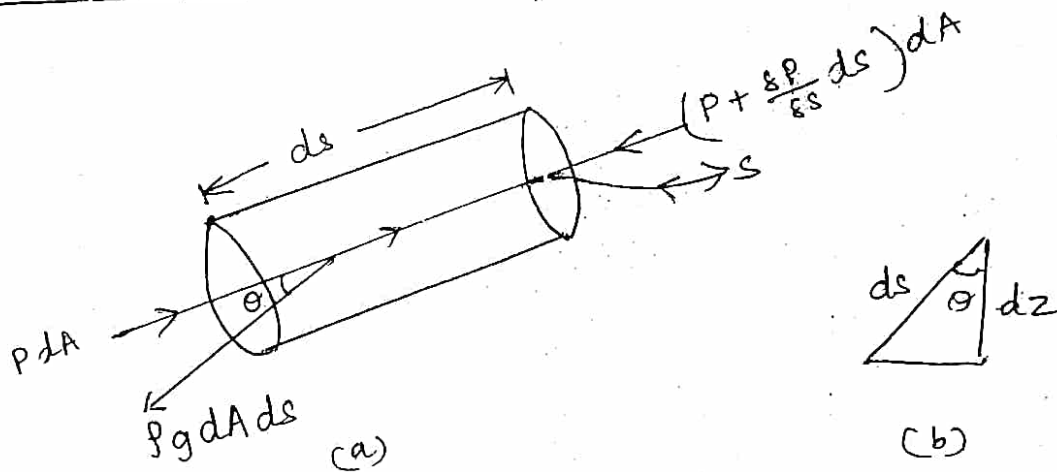
If the force due to compressibility F_c is negligible, the resulting net force,

$F_x = (F_g)_x + (F_p)_x + (F_v)_x + (F_t)_x$
 and equation of motions are called "Reynolds equations of motion".

(ii) For flow, where F_t is negligible, the resulting equation of motion are known as "Navier Stroke equation".

(iii) If the flow is assumed to be ideal, viscous force F_v is zero. and equation of motion are known as Eulers equation of motion.

Euler's Equation Of Motion:



In this equation the forces due to gravity and pressure are taken into consideration. Consider a stream in which flow is taking place in s direction as shown, in figure.

Consider the cylindrical element of cross section dA and length ds . The forces acting on the cylindrical element are

- (1) Pressure force $P \cdot dA$ in the direction of flow
- (2) Pressure force $(P + \frac{dp}{ds} \cdot ds) dA$ opposite to the direction of flow.

3) weight of the element $\rho g dA \cdot ds$

Let θ be angle between direction of flow and line of action of weight of the element

Resultant force on the element in the direction of flow S

$$S = (\text{mass of fluid element}) \times (\text{acceleration in direction } S)$$

$$\therefore P dA - \left(P + \frac{\delta P}{\delta s} \cdot ds \right) dA - \rho g dA \cos \theta \cdot ds = \rho dA \cdot ds \cdot a_s \quad \text{--- (2)}$$

where a_s is the acceleration in the direction of s .

Now $a_s = \frac{dv}{dt}$, where v is the function of s and t .

$$= \frac{dv}{ds} \cdot \frac{ds}{dt} + \frac{\delta v}{\delta t}$$

$$a_s = v \cdot \frac{\delta v}{\delta s} + \frac{\delta v}{\delta t}$$

$$\therefore \frac{ds}{dt} = v$$

If the flow is steady, $\frac{\delta v}{\delta t} = 0$

$$\therefore a_s = v \cdot \frac{\delta v}{\delta s}$$

Substituting the value of a_s in equation (2) and simplifying the equation, we get.

$$- \frac{\delta P}{\delta s} \cdot ds \cdot dA + P dA - P dA - \rho g dA \cos \theta \cdot ds = \rho \cdot dA \cdot ds \cdot v \cdot \frac{\delta v}{\delta s}$$

Dividing by $\rho dA \cdot ds$.

$$- \frac{1}{\rho} \frac{\delta P}{\delta s} - g \cos \theta = v \cdot \frac{\delta v}{\delta s}$$

From fig(b)
 $\therefore \cos \theta = \frac{dz}{ds}$

$$\text{or } \frac{1}{\rho} \frac{\delta P}{\delta s} + g \cdot \frac{dz}{ds} + v \cdot \frac{\delta v}{\delta s} = 0$$

$$\text{or. } \frac{dP}{\rho} + g \cdot dz + v \cdot dv = 0 \longrightarrow \textcircled{3}$$

Equation $\textcircled{3}$ is known as Euler's equation of motion.

Bernoulli's Equation from Euler's Equation

Bernoulli's equation is obtained by integrating the Euler's equation of motion $\textcircled{3}$ as..

$$\int \frac{dP}{\rho} + \int g \cdot dz + \int v \cdot dv = \text{constant}$$

If the flow is incompressible, ρ is constant and

$$\frac{P}{\rho} + gz + \frac{v^2}{2} = \text{constant}$$

Divide by g throughout

$$\frac{P}{\rho g} + z + \frac{v^2}{2g} = \text{constant} \longrightarrow \textcircled{4}$$

Equation $\textcircled{4}$ is called Bernoulli's equation in which,

$\frac{P}{\rho g}$ = Pressure energy per unit weight of fluid or pressure head

$\frac{v^2}{2g}$ = Kinetic energy per unit weight or kinetic head.

z = potential energy per unit weight or potential head.

Statement of Bernoulli's Theorem:

It states that in a steady, ideal flow of an incompressible fluid, the total energy at any point of the fluid is constant. The total energy consists of pressure energy, kinetic energy and potential energy or datum energy.

These energies per unit weight of the fluid are

$$\text{Pressure energy} = \frac{P}{\rho g}$$

$$\text{Kinetic energy} = \frac{v^2}{2g}$$

$$\text{Datum energy} = z$$

Thus mathematically Bernoulli's theorem is written as

$$\frac{P}{\rho g} + \frac{v^2}{2g} + z = \text{constant.}$$

Assumptions

The following assumptions are made in the derivation of Bernoulli's equation

- (1) Fluid is ideal i.e. viscosity is zero
- (2) Flow is steady and continuous
- (3) Flow is incompressible
- (4) Flow is irrotational
- (5) The flow is along the streamline, i.e. it is one dimensional.
- (6) The velocity is uniform over the section and is equal to mean velocity
- (7) The only forces acting on fluid are gravity and pressure forces.

.....

MODULE - 4

ORIFICE AND MOUTHPIECE

INTRODUCTION :

"An orifice" is an opening in the wall or base of a vessel through which the fluid flows. The top edge of the orifice is always below the free surface (If the free surface is below the top edge of the orifice, becomes a weir).

"A mouthpiece" is an attachment in the form of a small tube or pipe fixed to the orifice (the length of pipe extension is usually 2 to 3 times the orifice diameter) and is used to increase the amount of discharge.

Orifices and mouthpieces are used to measure the discharge or rate of flow.

Classification of Orifices :

The orifices are classified as follows :

1. According to size :

(i) Small orifice

(ii) Large orifice

An orifice is termed as small when its dimensions are small compared to the head causing flow. The velocity does not vary appreciably from top to the bottom edge of the orifice and is assumed to be uniform.

The orifice is large if the dimensions are comparable with the head causing flow. The variation in the velocity from the top to the bottom edge is considerable.

"If the head of liquid from the centre of orifice is ~~more~~ than five times the depth of orifice it is called small

Limitations of Bernoulli's equation:-

- (1) Curved Path: If the fluid is flowing in a curved path, the energy due to centrifugal force should also be considered.
- (2) Heat: If heat is added or taken from the fluid between the initial and final points and especially if there is a change of state from liquid to vapour or the reverse, the additional terms representing the intrinsic thermal energy per unit weight of the fluid must be added to both the sides of Bernoulli's equation.
- (3) Machine: If there is machine in a pipeline to add or subtract energy Ex a pump or reaction turbine, the heat added or subtracted by machine must be included as another term in Bernoulli's equation.
- (4) Types of flow: The Bernoulli's theorem applied along any laminar or stream line flow of a liquid at constant density and temperature when acted upon by no outside forces except gravity.

" If the head of liquid is less than five times the depth of orifice, it is known as large orifice".

2. According to shape:

i) Circular orifice

iii) Square orifice

ii) Rectangular orifice

iv) Triangular orifice

3. Shape of upstream edge:

i) Sharp-edged orifice



ii) Bell-mouthed orifice



4. According to discharge conditions:

i) Free discharge orifices

ii) Drowned or submerged orifices

(a) Fully submerged

(b) Partially submerged



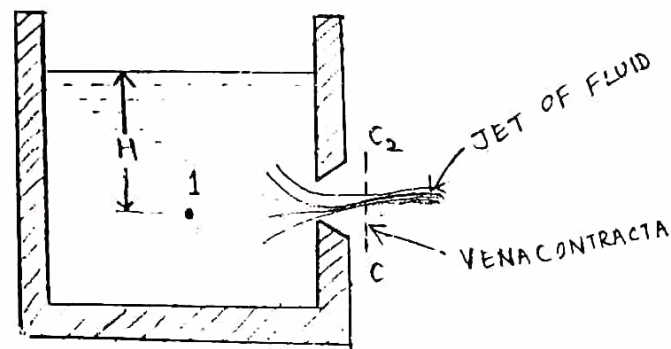
Note: An orifice or a mouthpiece is said to be discharging free when it discharges into atmosphere. It is said to be submerged when it discharges into another liquid.

5. Based on position: (i) Side of vessel wall (ii) Bottom of vessel

FLOW THROUGH AN ORIFICE

Consider a tank fitted with a circular orifice in one of its sides as shown in Fig. Let H be the head of the liquid above the centre of the orifice. The liquid flowing through the orifice forms a jet of liquid whose area of cross section is less than that of orifice. The area of jet of fluid goes on decreasing and at a section C-C, the area is minimum. This section is approximately at a distance of half of diameter of the

of the orifice. At this section, the streamlines are straight and parallel to each other and perpendicular to the plane of the orifice. This section is called Vena contracta. Beyond this section, the jet diverges and is attracted in the downward direction by the gravity.



TANK WITH AN ORIFICE

Consider two points 1 and 2 as shown in Fig. Point 1 is inside the tank and point 2 at the vena contracta. Let the flow is steady and at a constant head H . Applying Bernoulli's equation at points 1 and 2.

$$\frac{P_1}{\rho g} + z_1 + \frac{V_1^2}{2g} = \frac{P_2}{\rho g} + z_2 + \frac{V_2^2}{2g}$$

But $z_1 = z_2$

$$\therefore \frac{P_1}{\rho g} + \frac{V_1^2}{2g} = \frac{P_2}{\rho g} + \frac{V_2^2}{2g}$$

Now $\frac{P_1}{\rho g} = H$

$$\frac{P_2}{\rho g} = 0 \text{ (atmospheric pressure)}$$

V_1 is very small in comparison to V_2 as area of tank is very large as compared to the area of the jet of liquid

$$H + 0 = 0 + \frac{V_2^2}{2g}$$

$$\Rightarrow \boxed{V_2 = \sqrt{2gH}} \quad \text{②}$$

Actual velocity will be less than

HYDRAULIC COEFFICIENTS:

The hydraulic coefficients are:-

1. Coefficient of velocity, C_v
2. Coefficient of contraction, C_c
3. Coefficient of discharge C_d

1. Coefficient of velocity (C_v):

It is defined as the ratio between the actual velocity of a jet of liquid at vena contracta and the theoretical velocity of jet. $C_v = \frac{\text{Actual velocity of jet at Vena contracta}}{\text{Theoretical velocity}}$

$$= \frac{V}{\sqrt{2gH}}$$

where $V =$ actual velocity ; $\sqrt{2gH} =$ Theoretical velocity

The value of C_v varies from 0.95 to 0.99 for different orifices, depending on the shape, size of the orifice, and on the head under which flow takes place.

Generally value of $C_v = 0.98$ is taken for sharp edged orifices.

2. Coefficient of contraction (C_c):

It is defined as the ratio of the area of jet at vena contracta to area of the orifice.

$$C_c = \frac{\text{area of jet at vena contracta}}{\text{area of orifice}}$$

$$C_c = \frac{a_c}{a_o}$$

The value of C_c varies from 0.61 to 0.69 depending

Experimental Determination of Hydraulic Coefficients

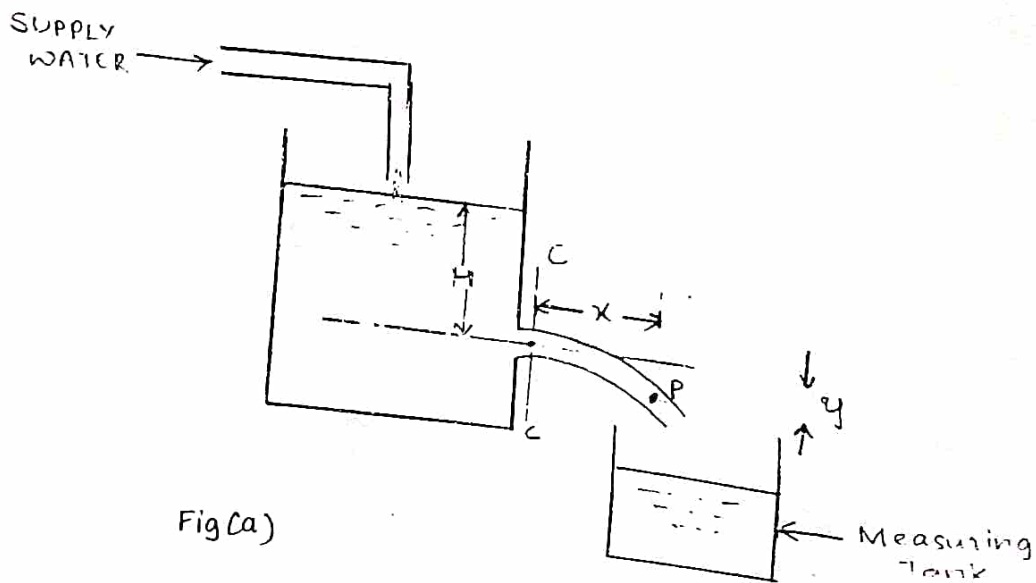
Determination of coefficient of Discharge (C_d):

The water is allowed to flow through an orifice from a tank under constant head H as shown in fig. The water is collected in a measuring tank for a known time t . The height of water in measuring tank is noted down. Then actual discharge through orifice,

$$Q = \frac{\text{Area of measuring tank} \times \text{Height of water in measuring tank}}{\text{Time}}$$

Theoretical discharge = area of orifice $\times \sqrt{2gH}$

$$C_d = \frac{Q}{a \times \sqrt{2gH}}$$



Fig(a)

Determination of coefficient of velocity (C_v)

Let C-C represents the vena contracta of jet of water coming out from an orifice under constant head H as shown in Fig(a). Consider a liquid particle which is at vena contracta at any time and takes the position at P along the jet in time ' t '

on shape and size of the orifice and head of liquid under which water flow takes place. In general, value of C_c may be taken as 0.64.

3. Coefficient of Discharge (C_d):

It is defined as the ratio of the actual discharge from an orifice to the theoretical discharge from the orifice.

$$C_d = \frac{Q}{Q_{th}} = \frac{\text{Actual discharge}}{\text{Theoretical discharge}}$$
$$= \frac{\text{Actual velocity} \times \text{Actual area}}{\text{Theoretical velocity} \times \text{Theoretical area}}$$

$$C_d = C_v \times C_c$$

The value of C_d varies from 0.61 to 0.65.
For general purpose C_d is taken as 0.62.

4. Coefficient of Resistance (C_r)

The ratio of loss of head (or loss of kinetic energy) in the orifice to the head of water (actual kinetic energy) available at the exit of the orifice is known as coefficient of resistance.

$$C_r = \frac{\text{Loss of head in the orifice}}{\text{Head of water}}$$

The loss of head in the orifice takes place, because the walls of the orifice offer some resistance to the liquid as it comes out. While solving the numerical problems C_r is generally neglected.

Module - 5

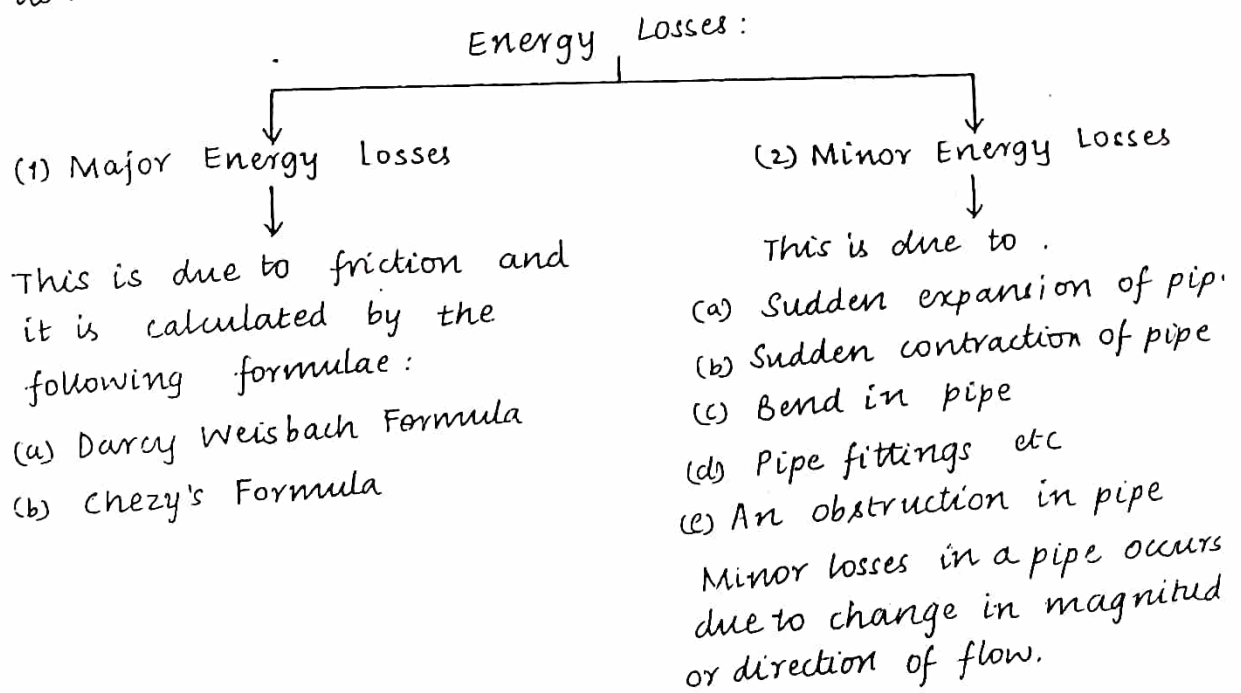
Introduction:

The term pipe is used to indicate the closed conduit which is used for carrying the fluids under pressure. Such a flow is known as a pipe flow.

The pipes always run full because they carry the fluid under pressure. Thus, the flow in a pipe which does not run full cannot be treated as a pipe flow.

Loss of Energy or Head in Pipes :

When a fluid is flowing through a pipe, the fluid experiences some resistance due to which some of the energy of fluid is lost. This loss of energy is classified as :-



Loss of Energy due to Friction:

(a) Darcy Weisbach Formula :-

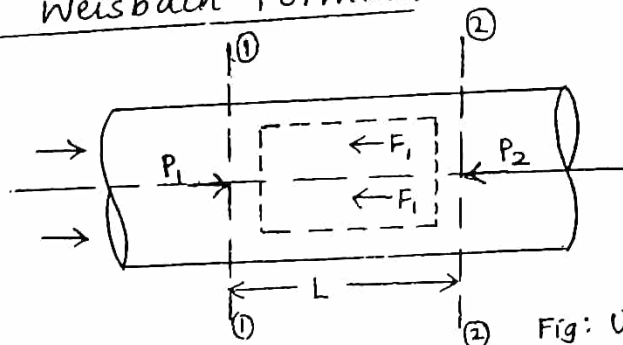


Fig: Uniform Horizontal Pipe

$$F_f = f' \times \pi d L \times v^2$$

$$= f' \times P \times L \times v^2$$

$$\left[\begin{array}{l} \text{Wetted area} = \pi d \times L \\ \text{velocity} = v = v_1 = v_2 \\ \text{Perimeter } P = \pi d \end{array} \right]$$

Forces acting on the fluid between section 1-1 and 2-2 are

(1) Pressure force at section 1-1 = $P_1 \times A$
 where A = Area of pipe

(2) Pressure force at section 2-2 = $P_2 \times A$

(3) Frictional force F_f

Resolving the forces in the horizontal direction, we have

$$P_1 A - P_2 A - F_f = 0$$

$$(P_1 - P_2) A = F_f$$

$$(P_1 - P_2) A = f' \times \pi d L \times v^2$$

$$(P_1 - P_2) = \frac{f' \times \pi d L \times v^2}{A}$$

From Equation (1), $P_1 - P_2 = \rho g h_f$

$$\rho g h_f = \frac{f' \times \pi d L \times v^2}{A} = \frac{f' \times P \times L \times v^2}{A}$$

$$P = \pi d$$

= Perimeter

$$h_f = \frac{f'}{\rho g} \times \frac{P}{A} \times L \times v^2 \longrightarrow (3)$$

In equation (3) $\frac{P}{A} = \frac{\text{Wetted Perimeter}}{\text{Area}} = \frac{\pi d}{\pi d^2/4} = \frac{4}{d}$

$$h_f = \frac{f'}{\rho g} \times \frac{4}{d} \times L \times v^2 \longrightarrow (4)$$

Putting $\frac{f'}{\rho} = \frac{f}{2}$, where f is known as coefficient of friction or friction factor

Equation (4) becomes $h_f = \frac{4 f L v^2}{2 g d} \longrightarrow (5)$

where $f = \frac{16}{Re}$ For ($Re < 2000$); $f = \frac{0.079}{Re^{1/4}}$ for ($Re > 4000$)

Consider a uniform horizontal pipe having flow as shown in fig. Let 1-1 and 2-2 are two sections of pipe.

Let P_1 = Pressure intensity at section 1-1

V_1 = Velocity of flow at section 1-1

L = Length of the pipe between sections 1-1 and 2-2.

d = diameter of pipe

f' = frictional resistance per unit wetted area per unit velocity

h_f = Loss of head due to friction

and P_2, V_2 are values of pressure intensity and velocity at section 2-2.

Applying Bernoulli's equation between sections 1-1 and 2-2
 (Total head at 1-1) = (Total head at 2-2) + (Loss of head due to friction between 1-1 and 2-2)

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + z_2 + h_f$$

But $z_1 = z_2$, since the pipe is horizontal.

$V_1 = V_2$ as diameter of pipe is same at 1-1 and 2-2.

$$\therefore \frac{P_1}{\rho g} = \frac{P_2}{\rho g} + h_f$$

$$h_f = \frac{P_1}{\rho g} - \frac{P_2}{\rho g} \longrightarrow \textcircled{1}$$

But h_f is the head loss due to friction and hence intensity of pressure will be reduced in the direction of flow by frictional resistance.

Now frictional resistance

$$= \left(\text{frictional resistance per unit wetted area per unit velocity} \right) \times \left(\text{wetted area} \right) \times \left(\text{velocity} \right)^2$$

Equation (5) is known as Darcy Weisbach equation. This equation is commonly used for finding loss of head due to friction in pipes. Consider
this

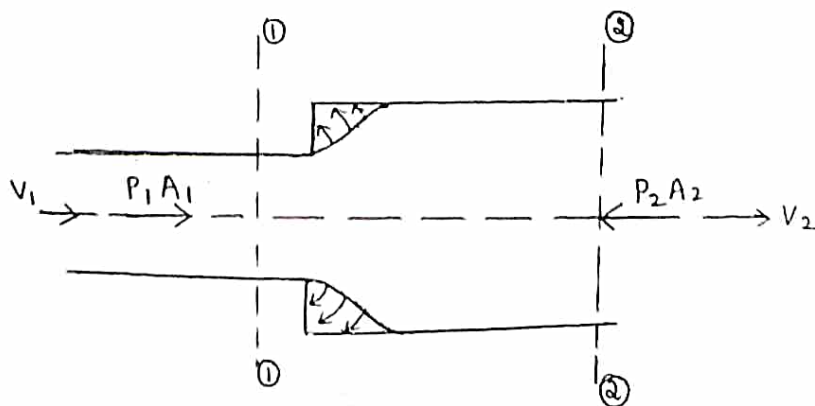
Minor Energy (Head) Losses :-

The loss of head due to friction in a pipe is known as major loss while the loss of energy due to change in velocity of the flowing fluid in magnitude or direction is called minor loss of energy. The minor loss of energy includes following cases :-

- (1) Loss of head due to sudden enlargement
- (2) Loss of head due to sudden contraction
- (3) Loss of head at the entrance of pipe
- (4) Loss of head at the exit of pipe
- (5) Loss of head due to an obstruction in a pipe
- (6) Loss of head due to bend in the pipe
- (7) Loss of head in various pipe fittings

In case of long pipes the above losses are small when compared with the loss of head due to friction. and hence they are called minor losses and even may be neglected without serious error. But in case of short pipe, these losses are comparable with the loss of head due to friction.

Loss of head Due to Sudden Enlargement



Consider a liquid flowing through a pipe which has a sudden enlargement as shown in figure.

Consider 2 sections (1-1) and (2-2) before and after the enlargement. Let P_1 = pressure intensity at section (1-1)

A_1 = Area of pipe at section (1-1)

V_1 = velocity of flow at section (1-1)

P_2, A_2, V_2 are corresponding values at section (2-2).

Due to sudden change of diameter of pipe from d_1 to d_2 . The liquid flowing from smaller pipe is not able to follow the abrupt change of boundary. Thus the flow separates from boundary and turbulent eddies are formed as shown in figure. The loss of head takes place due to formation of these eddies. Let P' is the pressure intensity of liquid eddies on the area $(A_2 - A_1)$. h_{-e} is the loss of head due to sudden expansion.

Applying Bernoulli's equation between section (1-1) and (2-2)

$$\frac{P_1}{w} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{w} + \frac{V_2^2}{2g} + z_2 + h_e$$

But $z_1 = z_2$ As pipe is horizontal

$$\frac{P_1}{w} + \frac{V_1^2}{2g} = \frac{P_2}{w} + \frac{V_2^2}{2g} + h_e$$

$$h_e = \frac{(P_1 - P_2)}{w} + \frac{(V_1^2 - V_2^2)}{2g} \quad \rightarrow \textcircled{1}$$

Consider the control volume of liquid between sections (1-1) and (2-2)

Force acting on the liquid in the control volume in the direction of flow is given by,

$$F_x = P_1 A_1 + P' (A_2 - A_1) - P_2 A_2$$

But experimentally it was found that $P' = P_1$

$$h_e = \frac{P_1 - P_2}{w} + \frac{(V_1^2 - V_2^2)}{2g}$$

From ⑤ we know $\frac{P_1 - P_2}{w} = \frac{V_2^2 - V_2 V_1}{g}$

$$h_e = \frac{V_2^2 - V_2 V_1}{g} + \frac{V_1^2 - V_2^2}{2g}$$

$$= \frac{2V_2^2 - 2V_1 V_2 + V_1^2 - V_2^2}{2g}$$

$$h_e = \frac{V_2^2 + V_1^2 - 2V_1 V_2}{2g}$$

$$h_e = \frac{(V_1 - V_2)^2}{2g}$$

Note :-

1) Loss of head due to sudden Enlargement

$$h_e = \frac{(V_1 - V_2)^2}{2g}$$

2) Loss of head due to sudden contraction

$$h_c = \frac{0.5 V_2^2}{2g} \quad \text{if } C_c \text{ [coefficient of contraction] is given}$$

$$h_c = \frac{k V_2^2}{2g} \quad \text{where } k = \left(\frac{1}{C_c} - 1 \right)^2$$

3) Loss of head at the entrance of pipe

$$h_i = \frac{0.5 V_1^2}{2g}$$

4) Loss of head at the exit of pipe

$$h_o = \frac{V_2^2}{2g}$$

5) Loss of head due to obstruction in pipe

$$= \frac{V^2}{2g} \left[\frac{A}{4(A-a)} - 1 \right]^2$$

$$F_x = P_1 A_1 + P_1 (A_2 - A_1) - P_2 A_2$$

$$F_x = (P_1 - P_2) A_2 \longrightarrow \textcircled{2}$$

Net force = Rate of change of momentum

$$= \left(\text{Momentum of liquid per sec at section (2-2)} \right) - \left(\text{Momentum of liquid per sec at section 1-1} \right)$$

Momentum of liquid per sec at section 1-1 = $\left(\frac{\text{Mass}}{\text{sec}} \right) \times \text{velocity}$

$$= (\rho A_1 v_1) \times v_1$$

$$= \rho A_1 v_1^2$$

Similarly momentum of liquid per second at section 2-2 } = $\left(\frac{\text{Mass}}{\text{sec}} \right) \times \text{velocity}$

$$= (\rho A_2 v_2) \times v_2$$

\therefore Rate of change of momentum = $\rho A_2 v_2^2$

$$= \rho A_2 v_2^2 - \rho A_1 v_1^2 \longrightarrow \textcircled{3}$$

By continuity equation $Q = A_1 v_1 = A_2 v_2$

$$A_1 = \left(\frac{v_2}{v_1} \right) \times A_2$$

\therefore Equation $\textcircled{3}$ becomes

change of momentum/second = $\rho A_2 v_2^2 - \rho \left(\frac{v_2}{v_1} \right) A_2 v_1^2$

$$= \rho A_2 (v_2^2 - v_1 v_2) \longrightarrow \textcircled{4}$$

Equating $\textcircled{2}$ and $\textcircled{4}$

$$(P_1 - P_2) A_2 = \rho A_2 (v_2^2 - v_1 v_2)$$

Divide both sides by g

$$\frac{P_1 - P_2}{\rho g} = \frac{v_2^2 - v_1 v_2}{g}$$

$$\frac{P_1 - P_2}{\rho} = \frac{v_2^2 - v_1 v_2}{g} \longrightarrow \textcircled{5}$$



Note : Answer any one full question from each Part.

| Q. No. | Question | Marks | Level | Course/Subject |
|-----------------|---|-------|-------|----------------|
| MODULE 2 | | | | |
| 3 a. | Derive the expressions for total pressure and centre of pressure for a plane surface submerged vertically in a liquid | 07 | L2 | C |
| b. | Determine the total force and location of centre of pressure for a circular plate of 2 m diameter immersed vertically in water with its top edge 1.0 m below the water surface
<i>2.125 m.</i> | 08 | L3 | C |
| OR | | | | |
| 4 a. | Derive an expression for Continuity Equation for three dimensional flow | 05 | L2 | C |
| b. | Distinguish between 1. Steady and unsteady flow
2. uniform and non-uniform flow | 03 | L1 | C |
| c. | The velocity field in a fluid is given by,
$\mathbf{V} = (3x + 2y)\mathbf{i} + (2z + 3x^2)\mathbf{j} + (2t - 3z)\mathbf{k}$ i. Determine the velocity components u , v , and w ?
ii. Determine the speed at the point (1,1,1).
iii. Determine the speed at time $t=2$ s at point (0,0,2)

$u = (3x + 2y)$, $v = (2z + 3x^2)$, $w = (2t - 3z)$ <i>4.472 units</i> | 07 | L3 | C |

| RBT (Revised Bloom's Taxonomy) Levels : Cognitive Domain | | |
|--|--------------------|---------------|
| L1 : Remembering | L2 : Understanding | L3 : Applying |
| L4 : Analysing | L5 : Evaluating | L6 : Creating |

Shanathra R.M.
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| | | | | | | | | | |
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| | | | |
|----------------------|-----------------|---------------------|-----------|
| Course/Subject Title | Fluid Mechanics | Course/Subject Code | 18CV33 |
| Semester | III - A | Scheme | CBCS - 18 |
| Date | 08.12.2020 | CIE No. | 1 |
| Time | 9 to 10 AM | Max. Marks | 30 |

| | |
|--|--|
| Course Outcome Statements : After the successful completion of the course, the students will be able to | |
| CO1 | Explain the fundamental properties of fluids |
| CO2 | Explain the concept of fluid pressure and equipment for its measurement |
| CO3 | Calculate the hydrostatic forces acting on surfaces and explain the kinematic concepts of fluid flow |
| CO4 | Apply Euler's equation and Bernoulli's principle for the practical applications of fluid flow |
| CO5 | Compute the discharge through channels and pipes |
| CO6 | Explain the losses in pipe flow and effect of water hammer in pipe flow |

Note : Answer any one full question from each Part.

| Q. No. | Question | Marks | RBT Level | CO |
|---|--|---|-----------|-----|
| MODULE 1 | | | | |
| 1 a. | Define the following fluid properties with units i) Mass density, ii) Specific gravity iii) Dynamic Viscosity, iv) Vapour pressure v) Capillarity | 10 | L1 | CO1 |
| b. | Define absolute pressure, vacuum pressure and gauge pressure with a neat sketch showing the relationship between them | 5 | L1 | CO2 |
| OR | | | | |
| 2 a. | Write a note on i) Piezometer ii) U-tube manometer and iii) Differential manometer | 6 | L1 | CO2 |
| b. | Figure 1 shows a conical vessel having its outlet A to which a U-tube manometer is connected. The reading of the manometer given in the figure shows when the vessel is empty. Determine the reading of manometer when the vessel is completely filled with water. | 9 | L3 | CO2 |
| OR | | | | |
| In Figure2, the air pressure in the left tank is 230mm of mercury (Vacuum). Determine height h in the right limb shown, if the liquid in the right tank is water. | | | | |
| <p style="text-align: center;">Mercury
Figure 1</p> | | <p style="text-align: center;">manometric liquid (S=1.6)
Figure 2</p> | | |

- c. A 300 mm diameter pipe carries water under a head of 20 m with a velocity of 3.5 m/s. If the axis of the pipe turns through 45° . Find the magnitude and direction of the resultant force at the bend. (08 Marks)

OR

- 6 a. Derive the equation for discharge through venturimeter. (08 Marks)
 b. A venturimeter is to be fitted in a pipe of 0.25 m diameter where the pressure head is 7.6 m of flowing liquid and the maximum flow is $8.1 \text{ m}^3/\text{minute}$. Find the diameter of the throat of the venturimeter. Take $C_d = 0.96$. (06 Marks)
 c. A pipeline carrying oil of specific gravity of 0.87 changes in diameter from 200 mm at a point A to 500 mm diameter at point B which is 4 m higher. If the pressure at A and B are 9.81 N/cm^2 and 5.886 N/cm^2 respectively and the discharge is 200 l/s . Determine the loss of head and direction of flow. (06 Marks)

Module-4

- 7 a. Define the hydraulic coefficients (C_c , C_d , C_v) of an orifice and obtain the relation between them. (06 Marks)
 b. Explain the classification of orifice and mouthpiece based on their shape, size, sharpness and discharge. (06 Marks)
 c. Water flows through a triangular right angled weir first and then over a rectangular weir of 1 m width. The C_d values of triangular and rectangular weir are 0.6 and 0.7 respectively. If the depth of water over the triangular weir is 360 mm, find the depth of water over the rectangular weir. (08 Marks)

OR

- 8 a. Explain Cipolletti notch. What is the advantage of Cipolletti notch over trapezoidal notch. (06 Marks)
 b. Water discharge at the rate of 98.2 litre/sec through a 20 mm diameter vertical sharp edged orifice placed under a constant head of 10 m. A point on the jet measured from the venacontracta of the jet has co-ordinate (4.5, 0.54). Find the coefficients C_c , C_v , C_d of the orifice. (08 Marks)
 c. Derive an expression for discharge through a V notch. (06 Marks)

Module-5

- 9 a. Explain major and minor losses in a pipe flow. Give an expression for head loss due to sudden expansion in pipe flow. (08 Marks)
 b. Three pipes of lengths 800 m, 500 m and 400 m and of diameters 500 mm, 400 mm and 300 mm respectively are connected in series. These pipes are to be replaced by a single pipe of length 1700 m. Find the diameter of the single pipe. (06 Marks)
 c. What is the maximum permissible velocity in a cast iron pipeline 10 mm diameter and 15 mm thick which can be suddenly stopped by a valve at the outlet end of the pipe without letting the rise of pressure in the pipe to exceed $1.545 \times 10^3 \text{ kN/m}^2$.
 Take E for cast iron = $123.606 \times 10^9 \text{ N/m}^2$, K for water = $206.01 \times 10^7 \text{ N/m}^2$. Neglect effect of Poisson's ratio. (06 Marks)

OR

- 10 a. Define the term compound pipe and equivalent pipe. Derive the expression for diameter of equivalent pipes. (06 Marks)
 b. Explain Hardy cross method used in pipe networks. (06 Marks)
 c. The population of a city is 8,00,000 and it is to be supplied with water from a reservoir 6.4 km away. Water is to be supplied at the rate of 140 litres per head per day and half the supply is to be delivered in 8 hours. The full supply level of the reservoir is RL 180.00 and its lowest water level is RL 105.00. The delivery end of the main is at RL 22.50 and the head required there is 12 m. Find the diameter of the pipe. Take $f = 0.04$. (08 Marks)

* * *

704



Bapuji Educational Association ®
Bapuji Institute of Engineering and Technology, Davangere-577 004
Department of Civil Engineering

| | | | |
|----------------------|-----------------|---------------------|-----------|
| Assignment No. | 1 | Maximum Marks | 10 |
| Course/Subject Title | FLUID MECHANICS | Course/Subject Code | 18CV33 |
| Semester | III A | Scheme | CBCS - 18 |
| Course Co-ordinator | Sharathraj R M | | |

| | |
|--|--|
| Course Outcome Statements : After the successful completion of the course, the students will be able to | |
| CO1 | Explain the fundamental properties of fluids |
| CO2 | Explain the concept of fluid pressure and equipment for its measurement |
| CO3 | Calculate the hydrostatic forces acting on surfaces and explain the kinematic concepts of fluid flow |
| CO4 | Apply Euler's equation and Bernoulli's principle for the practical applications of fluid flow |
| CO5 | Compute the discharge through channels and pipes |
| CO6 | Explain the losses in pipe flow and effect of water hammer in pipe flow |

Note : Answer all the questions.

| Q. No. | Question | Marks | RBT Level | CO |
|--------|---|-------|-----------|----|
| 1 | Define absolute pressure, vacuum pressure and gauge pressure with a neat sketch showing the relationship between them | 2.5 | L2 | 1 |
| 2 | Write a note on mechanical gauges | 2.5 | L2 | 2 |
| 3 | Explain Eulerian and Lagrangian approach of fluid motion | 2.5 | L2 | 3 |
| 4 | List methods of drawing Flow net and explain any two | 2.5 | L2 | 3 |

| | | | |
|---------------------------------|-----------|-----------|-------------|
| Last date for submission | 15 | 12 | 2020 |
|---------------------------------|-----------|-----------|-------------|

| | | |
|---|--------------------|---------------|
| RBT (Revised Bloom's Taxonomy) Levels : Cognitive Domain | | |
| L1 : Remembering | L2 : Understanding | L3 : Applying |
| L4 : Analysing | L5 : Evaluating | L6 : Creating |

Sharathraj R.M
11/12/2020
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Program Coordinator
(HOD, Civil)



Scheme of Valuation



2. a) Piezometer: device used to measure liquid pressure in a system by measuring height to which column of liquid rises against gravity. → 2

U-tube manometer,

to measure the pressure difference in fluid or orifice located in the airflow in air handling or ventilation system. → 2

Differential manometer is a device that measure the difference in pressure between two places with figure or explanation. → 2

Types.

- * Two piezometer manometer,
- * Inverted U tube manometer & micro manometer.

b) problem.

solution.

$$h_B = 230 \text{ mm of Hg} = 0.23 \times 13.6 = -3.128 \text{ m of water}$$

$$h_C = \frac{P_C}{\rho} = \frac{21}{9.81} = 2.14 \text{ m of water} \quad \rightarrow 2$$

$$-3.128 + 5 \times 0.8 + y \times 1.6 - (y + 2) = 2.14$$

$$-3.128 + 5 \times 0.8 + y \times 1.6 - y - 2 = 2.14 \quad \rightarrow 3$$

$$y = 5.446 \text{ m}$$

$$\therefore \text{Elevation of A} = 100 - 5.446$$

$$\text{Elevation of A} = 94.553 \text{ m} \quad \rightarrow 4$$

4.
3.07

6.

9



Scheme of Valuation

| | | | |
|----------------------|-----------------|---------------------|--------|
| Course/Subject Title | Fluid Mechanics | Course/Subject Code | 18CV33 |
| Semester | III - A. | CIE No. | I |
| Date | 8/12/2020. | Max. Marks | 30 |

1. a) Define Mass density. $\rho = \frac{\text{mass of fluid}}{\text{Volume of fluid}} = \frac{m}{V} \frac{\text{kg}}{\text{m}^3}$ + 2

Specific gravity = $\frac{\text{specific weight of fluid}}{\text{specific weight of standard fluid}}$.
 (G) + 2

$G_{\text{water}} = 1$, mercury = 13.6.

Dynamic viscosity $\mu = \frac{\tau}{du/dy}$ N.s/m² or Pascal. second. + 2

Vapour pressure
 a liquid will boil (vaporise) and is in equilibrium with its own vapour increases as temperature increases. + 2

Capillarity + rise or fall of liquid surface in a small tube relative to a general level of liquid when tube is held vertically in liquid. + 2

$h = \frac{4\sigma \cos\theta}{\rho g d}$

10.

b) Absolute pressure is at a point the intensity of pressure at the point measured with reference to absolute vacuum or absolute zero pressure + 2

+ It can never be negative or zero

5.

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 (Faculty in charge)

Dr. J. S. Rao
 Coordinator
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 Program Coordinator
 (HOD, Civil)
 8/12/20

USN

| | | | |
|----------------------|-------------------|---------------------|-----------|
| Course/Subject Title | Fluid Mechanics | Course/Subject Code | 18CV33 |
| Semester | III - A | Scheme | CBCS - 18 |
| Date | 04.01.2021 | CIE No. | II |
| Time | 11:30 to 12:30 AM | Max. Marks | 30 |

| | |
|--|--|
| Course Outcome Statements : After the successful completion of the course, the students will be able to | |
| CO1 | Explain the fundamental properties of fluids |
| CO2 | Explain the concept of fluid pressure and equipment for its measurement |
| CO3 | Calculate the hydrostatic forces acting on surfaces and explain the kinematic concepts of fluid flow |
| CO4 | Apply Euler's equation and Bernoulli's principle for the practical applications of fluid flow |
| CO5 | Compute the discharge through channels and pipes |
| CO6 | Explain the losses in pipe flow and effect of water hammer in pipe flow |

Note : Answer any one full question from each Part.

| Q. No. | Question | Marks | RBT Level | CO |
|-----------------|--|-------|-----------|----|
| MODULE 3 | | | | |
| 1 a. | List applications of Bernoulli's equation, Derive the equation for discharge through Venturi meter | 7 | L1,L2 | 4 |
| b. | A pipe through which water is flowing having diameter 20cm and 10 cm at the cross section 1 and 2 respectively. The velocity of water at section 1 is given 4m/s Find the velocity head at section 1 and 2 and also rate of discharge | 8 | L3 | 4 |
| OR | | | | |
| 2 a. | State and prove Bernoulli's theorem for steady flow of incompressible fluid. | 7 | L1,L2 | 4 |
| b. | a pipe of 300mm diameter is conveying $0.3\text{m}^3/\text{s}$ of water has a right angled bend in horizontal plane. Find the resultant force exerted on the bend if the pressure at inlet and outlet of the bend are 24.525×10^4 Pa and 23.544×10^4 Pa respectively | 8 | L3 | 4 |
| MODULE 4 | | | | |
| 3 a. | Derive Darcy-Weisbach equation for head loss due to friction in pipe | 7 | L2 | 6 |
| b. | Find the head loss due to friction in a pipe of diameter 300mm and length 50m, through which water is flowing at a velocity 3 m/s using Darcy-Weisbach equation, take kinematic viscosity for water = 0.01 strokes | 8 | L3 | 6 |
| OR | | | | |
| 4 a. | Explain water hammer, Derive expression for water hammer due to sudden closure of valve and pipe is rigid | 7 | L2 | 6 |
| b. | List the energy losses in pipe flow, Derive equation for head loss due to sudden enlargement in pipe | 8 | L1,L2 | 6 |

Charathraj.R.M
30/12/2020

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Prasad

Program Coordinator
(HOD, Civil)



Scheme of Valuation

- 4.b) Steady flow → the fluid properties do not change with time (t) $\frac{\partial (P)}{\partial t} = 0$ → 1.5
- unsteady flow $\frac{\partial (P)}{\partial t} \neq 0$.
- uniform flow $\frac{\partial (P)}{\partial x} = 0$ → (P) do not change over length of flow considered.
- non uniform flow $\frac{\partial (P)}{\partial x} \neq 0$ → 1.5 3.

4(c). Given.

$$V = (3x + 2y) i + (2z + 3x^2) j + (2t - 3z) k.$$

i) $u = 3x + 2y$

$v = 2z + 3x^2$

$w = 2t - 3z$

velocity component x, y, z.

ii) substituting $x=1, y=1, z=1$ in expression

$$u = (3 \times 1 + 2 \times 1) = 5$$

$$v = (2 \times 1 + 3 \times 1) = 5$$

$$w = (2t - 3 \times 1) = (2t - 3)$$

$$v^2 = u^2 + v^2 + w^2$$

$$v^2 = 4t^2 - 12t + 5$$

at point (1, 1, 1).

iii) substituting

$$t=2, x=0, y=0, z=2.$$

$$u=0, v=4+0, w=4-6=-2$$

$$v^2(0, 0, 2) = 0^2 + 4^2 + (-2)^2 = 16 + 4 = 20$$

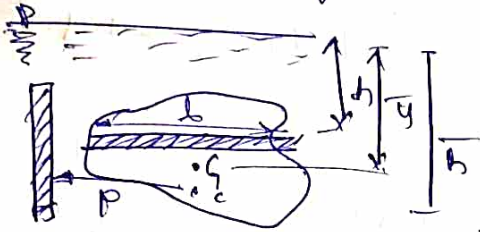
$$v = \sqrt{20} = 4.472$$

$$v = 4.472 \text{ units} \quad - 3 \quad 7.$$

Scheme of Valuation

3. a)

Hydrostatic forces on vertical plane surface



where
 A = Total area of surface
 \bar{y} = Depth of centroid from free surface
 G = centroid of immersed surface.
 C = centre of pressure.

$P = \rho g h$

$dP = (\rho g h) \cdot dA$

$\bar{y} = \frac{I_G}{Ay} + \bar{y}$

$A = \frac{\pi \times D^2}{4} = \frac{\pi \times 2^2}{4} = 3.142 \text{ m}$

$\rho = 1000 \text{ Kg/m}^3 \quad g = 10 \text{ m/s}^2$

$P = \rho g A \bar{y} = 1000 \times 10 \times 3.142 \times 2 = 62831 \text{ N}$

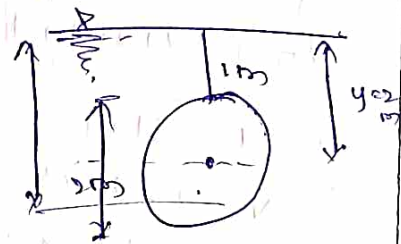
Centre of pressure

$\bar{h} = \bar{y} + \frac{I_G}{Ay}$ $I_G = \frac{\pi R^4}{4} = \frac{\pi \times 1^4}{4} = 0.785 \text{ m}^4$

$\bar{h} = 2 + \frac{0.785}{3.142 \times 2} = 2.125 \text{ m}$ $\bar{h} = 2.125 \text{ m}$

$P = \rho g A \bar{h} = \rho A \bar{h}$

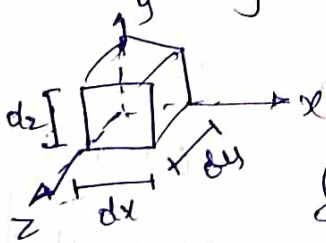
ρ = specific weight of water.



b)

4. a)

Continuity equation for 3 dimensional flow.



$dM_x = -\frac{\partial}{\partial x} (\rho u) dx dy dz$

dM_y, dM_z

$\frac{\partial (\rho u)}{\partial x} + \frac{\partial (\rho v)}{\partial y} + \frac{\partial (\rho w)}{\partial z} = 0$

7

8.

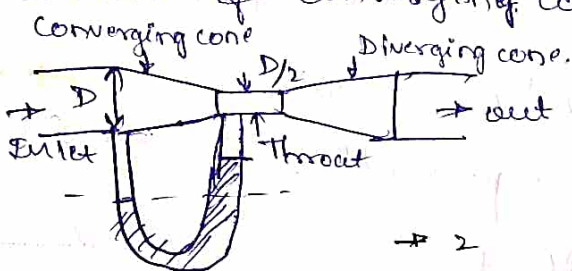
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Scheme of Valuation

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|----------------------|-----------------|---------------------|--------|
| Course/Subject Title | Fluid Mechanics | Course/Subject Code | 18CV33 |
| Semester | III.A. | CIE No. | II |
| Date | 04/01/2021 | Max. Marks | 30 |

1.a. Discharge through venturimeter :-
 A device used to measure rate of flow in pipe consists of converging cone, throat, diverging cone.



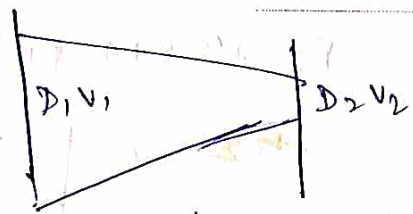
Bernoulli's equation.

$$\frac{P}{\rho g} + \frac{V^2}{2g} + Z = 0$$

$$Q_{act} = cd \frac{a_1 a_2}{\sqrt{a_1^2 - a_2^2}} \sqrt{2gh}$$

$$h = x \left[\frac{SH}{SL} - 1 \right], \quad h = x \left[1 - \frac{SL}{SH} \right]$$

b. Problem solution venturimeter, $Q_{th} = \frac{a_1 a_2}{\sqrt{a_1^2 - a_2^2}} \sqrt{2gh}$
 $D_1 = 20 \text{ cm} = 0.2 \text{ m}, \quad D_2 = 0.1 \text{ m}$



$$A_1 = \frac{\pi D_1^2}{4} = 0.0314 \text{ m}^2$$

$$A_2 = 0.00785 \text{ m}^2$$

continuity equation

$$Q_1 = Q_2$$

$$A_1 V_1 = A_2 V_2$$

$$V_2 = \frac{A_1 V_1}{A_2} = 16 \text{ m/s}$$

$$\frac{V_1^2}{2g} = \frac{4^2}{2 \times 9.81} = 0.815 \text{ m}$$

$$\frac{V_2^2}{2g} = \frac{16^2}{2 \times 9.81} = 83.047 \text{ m}$$

$$Q = A_1 V_1$$

$$= 0.0314 \times 4$$

$$= 0.1256 \text{ m}^3/\text{s}$$

$$Q = 125.6 \text{ litres/sec}$$

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Scheme of Valuation



2.a. Bernoulli's theorem. In a steady, incompressible flow the total energy remains constant at any point

$$\frac{P}{\rho g} + \frac{V^2}{2g} + z = \text{constant} \quad \rightarrow 2$$

pressure head + velocity head + datum head = constant
it is obtained from integration of Euler's equation

$$\int \frac{\partial P}{\rho} + \int g \cdot dz + \int v \cdot dv = \text{constant} \quad \rightarrow 2$$

if the flow is incompressible ρ is constant.

$$\frac{P}{\rho} + gz + \frac{V^2}{2} = \text{constant}$$

divide by g throughout.

$$\frac{P}{\rho g} + \frac{V^2}{2g} + z = \text{constant}$$

+ Bernoulli's equation

b). Pitot tube.

Data: $D_1 = D_2 = 300 \text{ mm}$

$P_1 = 24.525 \times 10^4 \text{ Pa}$ $P_2 = 23.544 \times 10^4 \text{ N/m}^2$

$Q = 0.3 \text{ m}^3/\text{s}$

$$V_1 = V_2 = \frac{Q}{A_1} = 4.24 \text{ m/s} \quad \rightarrow 2$$

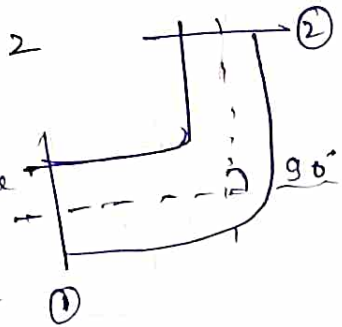
$$F_x = \rho Q (V_1 - V_2 \cos \theta) + P_1 A_1 - P_2 A_2 \cos \alpha$$

$$= 18606.27 \text{ N}$$

$$F_y = -17912.89 \text{ N} \quad \rightarrow 2$$

$$F = \sqrt{F_x^2 + F_y^2} = 25827.59 \text{ N}$$

$$\alpha = \tan^{-1} \left(\frac{F_y}{F_x} \right) = 43.89^\circ \quad \rightarrow 3.5$$



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DQAC

21/12/20
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3.5

7.5

7.5



Scheme of Valuation

| | |
|---------------------|--|
| Document No. | |
| Subject Title | |
| Master | |
| Course Co-ordinator | |
| Con | |

Water hammer in pipes:
In a long pipe when the flowing water is suddenly brought to rest by closing valve there will be sudden rise in pressure due to the momentum of water being destroyed. The sudden rise in pressure has effect of hammer action of walls of pipe. +3

Factors: \propto length, elastic properties of pipes, velocity of flow. +1

Sudden closure of valve in rigid pipe:

$$P = \frac{\rho L V}{T}, \quad P^2 = \rho K V^2$$

$$P = V \sqrt{\rho K}$$

$$P = V \sqrt{\frac{K \rho}{g}}$$

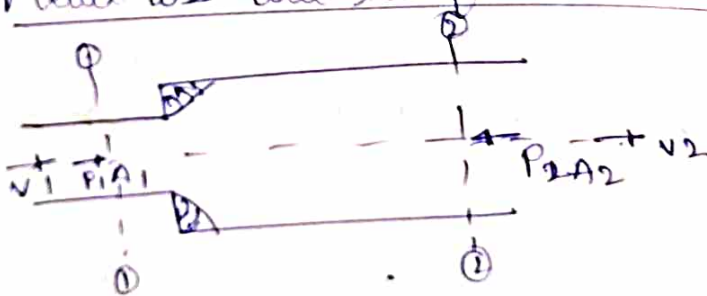
$$P = \rho V C$$

where

$$C = \sqrt{\frac{K}{\rho}} = \text{velocity of pressure wave.}$$

+3.5

Head loss due to sudden enlargement:-



+ minor losses.

+ Bernoulli's equation @ (1) and (2).

$$\frac{P_1}{\rho g} + \frac{v_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{v_2^2}{2g} + z_2 + h_e$$

$$z_1 = z_2$$

$$h_e = \frac{v_1^2 - v_2^2}{2g}$$

head loss due to sudden enlargement.

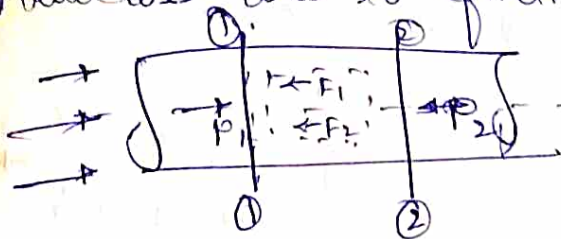
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Course Coordinator
(Faculty in charge)

Handwritten signature
Coordinator
D/O/A

Handwritten signature
Program Coordinator
D/O/A

Scheme of Valuation

3.9) Losses in pipe flow + major & minor loss
 Head loss due to friction + Darcy's weisbach eqn



Apply Bernoulli's eqn.
 at ①① & ②② +2

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + z_2 + (h_f) \rightarrow \text{head loss due to friction}$$

$$z_1 = z_2$$

$$V_1 = V_2$$

$$h_f = \frac{f_1}{\rho g} * \frac{P}{A} * L * V^2 \rightarrow ③$$

$$h_f = \frac{f_1}{\rho g} * \frac{4}{d} * L * V^2 \rightarrow ④$$

PETD.

$$\frac{f_1}{\rho} = \frac{f}{2}$$

$$h_f = \frac{4 f L V^2}{2 g d}$$

$$f = \frac{16}{Re} \quad \left. \begin{array}{l} Re < 2000 \\ \rightarrow 2 \end{array} \right\}$$

$$f = \frac{0.079}{R^{1/4}} \quad \left. \begin{array}{l} Re > 1000 \\ \rightarrow 3.5 \end{array} \right\}$$

3.6) problem

Data: Dia = d = 300mm = 0.3m, L = 50m, V = 3 m/s

$$\gamma = 0.01 \text{ cm}^2/\text{sec} = 0.01 \times 10^{-4} \text{ m}^2/\text{s} \quad \rightarrow 2$$

$$h_f = \frac{4 f L V^2}{2 g d}$$

$$Re = \frac{Vd}{\gamma} = 9 \times 10^5$$

$$h_f = \frac{4 \times 0.00256 \times 50 \times 3^2}{2 \times 9.81 \times 0.3}$$

$$f = \frac{0.079}{Re^{1/4}} = 0.00256 \quad \rightarrow 2$$

$$h_f = 0.7828 \text{ m} \quad \rightarrow 3.5 \quad 7$$

Ghorabhai Rm
 31/12/2020
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 (Faculty in charge)

Dr. S. S. S. S.
 Coordinator
 DOAC

2/1/2021
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 (HOD CIVIL)



Scheme of Valuation

| | | | |
|----------------------|-----------------|---------------------|--------|
| Course/Subject Title | FLUID MECHANICS | Course/Subject Code | 18CV33 |
| Semester | III Semester | CIE No. | III |
| Date | 102/2021 | Max. Marks | 30. |

1. Hydraulic coefficients:-

- a) 1. Co-efficient of velocity ($C_v = 0.98$)
 2. Co-efficient of contraction ($C_c = 0.61$ to 0.69)
 3. Co-efficient of discharge ($C_d = 0.61$ to 0.65)

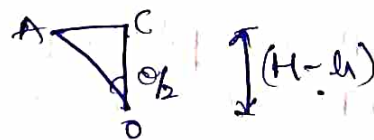
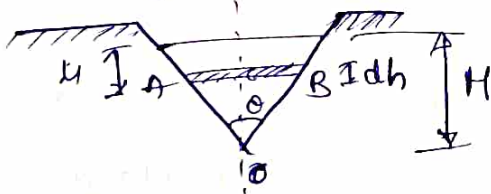
$C_v = \frac{\text{Actual velocity of jet @ vena contracta}}{\text{Theoretical velocity}} = \frac{V}{\sqrt{2gh}}$ → 3

$C_c = \frac{\text{Area of jet at vena contracta}}{\text{area of orifice}} = \frac{a_c}{a_o}$ → 3

$C_d = \frac{\text{Actual discharge}}{\text{Theoretical discharge}}$ → 3

$C_d = C_v \times C_c$ → 1.5

1. b) Triangular Notch.



$\tan \theta/2 = \frac{AC}{OC} = \frac{AC}{(H-h)}$

$AB = 2AC = 2(H-h) \tan \theta/2$ → 3

Area of strip = $2(H-h) \tan \theta/2 \times dh$

e. h. s. r. s. s.
 Course Coordinator (Faculty in charge)

Program Coordinator
 DQAC

Program Coordinator
 (HOD, Civil)



USN

| | | | |
|----------------------|-----------------|---------------------|-----------|
| Course/Subject Title | Fluid Mechanics | Course/Subject Code | 18CV33 |
| Semester | III – A | Scheme | CBCS – 18 |
| Date | 22/02/2021 | CIE No. | 03 |
| Time | 9 to 10 | Max. Marks | 30 |

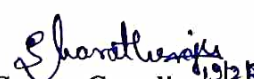
| | |
|--|--|
| Course Outcome Statements : After the successful completion of the course, the students will be able to | |
| CO1 | Explain the fundamental properties of fluids |
| CO2 | Explain the concept of fluid pressure and equipment for its measurement |
| CO3 | Calculate the hydrostatic forces acting on surfaces and explain the kinematic concepts of fluid flow |
| CO4 | Apply Euler's equation and Bernoulli's principle for the practical applications of fluid flow |
| CO5 | Compute the discharge through channels and pipes |
| CO6 | Explain the losses in pipe flow and effect of water hammer in pipe flow |

Note : Answer any one full question from each Part.

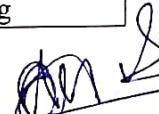
| Q. No. | Question | Marks | RBT Level | CO |
|---------------|--|-------|-----------|----|
| PART A | | | | |
| 1 a. | Explain different hydraulic coefficients and establish relation between them | 7.5 | L2 | 5 |
| b. | Derive an expression for discharge over Triangular notch | 7.5 | L2 | 5 |
| OR | | | | |
| 2 a. | The head of water over an orifice of diameter 40mm is 10 m, find actual discharge and actual velocity of jet at vena contracta ,take Cd=0.6 and Cv =0.98 | 7.5 | L3 | 5 |
| b. | Stating assumptions made , Derive the Eulers equation and hence obtain Bernoulis equation from it | 7.5 | L2 | 4 |
| PART B | | | | |
| 3 a. | What is Cipolletti notch and derive an expression for discharge over cipolletti notch | 7.5 | L2 | 5 |
| b. | For a Borda's mouthpiece (running free) show that Cc is 0.5 | 7.5 | L2 | 5 |
| OR | | | | |
| 4 a. | Find the discharge over a triangular notch of angle 60° when the head over the V notch is 0.3m assume Cd=0.6 | 7.5 | L3 | 5 |
| b. | Derive an expression for head loss due to friction in pipes | 7.5 | L2 | 6 |

RBT (Revised Bloom's Taxonomy) Levels : Cognitive Domain

| | | |
|------------------|--------------------|---------------|
| L1 : Remembering | L2 : Understanding | L3 : Applying |
| L4 : Analysing | L5 : Evaluating | L6 : Creating |


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(Faculty in charge)


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| | | | |
|----------------------|-----------------|---------------------|-----------|
| Segment No. | 2 | Maximum Marks | 10 |
| Course/Subject Title | FLUID MECHANICS | Course/Subject Code | 18CV33 |
| Semester | III A | Scheme | CBCS - 18 |
| Course Co-ordinator | Sharathraj R M | | |

Course Outcome Statements : After the successful completion of the course, the students will be able to

| | |
|------------|--|
| CO1 | Explain the fundamental properties of fluids |
| CO2 | Explain the concept of fluid pressure and equipment for its measurement |
| CO3 | Calculate the hydrostatic forces acting on surfaces and explain the kinematic concepts of fluid flow |
| CO4 | Apply Euler's equation and Bernoulli's principle for the practical applications of fluid flow |
| CO5 | Compute the discharge through channels and pipes |
| CO6 | Explain the losses in pipe flow and effect of water hammer in pipe flow |

Note : Answer all the questions.

| Q. No. | Question | Marks | RBT Level | CO |
|--------|--|-------|-----------|----|
| 1 | Write a note on Euler's equation of motion along stream line | 2.5 | L2 | 4 |
| 2 | List applications of Bernoulli's equation, Explain pitot tube | 2.5 | L2 | 4 |
| 3 | Explain network of pipes using Hardy cross method | 2.5 | L2 | 6 |
| 4 | Define water hammer, derive equation for pressure rise due to sudden closure of valve for elastic pipes. | 2.5 | L2 | 6 |

| | | | |
|---------------------------------|-----------|-----------|-------------|
| Last date for submission | 05 | 01 | 2021 |
|---------------------------------|-----------|-----------|-------------|

| RBT (Revised Bloom's Taxonomy) Levels : Cognitive Domain | | |
|--|--------------------|---------------|
| L1 : Remembering | L2 : Understanding | L3 : Applying |
| L4 : Analysing | L5 : Evaluating | L6 : Creating |

Sharathraj R.M
30/12/2020
Course Coordinator
(Faculty in charge)

Sharathraj R.M
Coordinator
DQAC

Sharathraj R.M
Program Coordinator
(HOD, Civil)



Scheme of Valuation

1. b) $Q = \frac{8}{15} C_d \sin \frac{\theta}{2} \sqrt{2g} H^{5/2}$
 for right angled v-notch, if $C_d = 0.6$
 $\theta = 90^\circ$ $\sin \frac{\theta}{2} = 1$
 $Q = \frac{8}{15} \times 0.6 \times 1 \times \sqrt{2 \times 9.81} \times H^{5/2} = 1.417 H^{5/2}$

2. a)

Solution:- ORIFICE

Given head = $H = 10m$, $d = 40mm = 0.04m$

Area, $a = \frac{\pi \times 0.04^2}{4} = 0.001256 m^2$ $C_d = 0.6$

$\frac{\text{Actual discharge}}{\text{Theoretical discharge}} = 0.6$ $C_v = 0.98$

$V_{th} = \sqrt{2gH} = \sqrt{2 \times 9.81 \times 10} = 14 m/s$

$Q_{th} = 14 \times 0.001256 = 0.01758 m^3/s$

$Q_d = 0.6 \times Q_{th} = 0.01054 m^3/s$

$\frac{\text{Actual velocity}}{\text{Theoretical velocity}} = C_v = 0.98$

Actual velocity = $C_v \times$ Theoretical velocity
 $= 0.98 \times 14 = 13.72 m/s$

2. b) Assumptions :-

- + Fluid is ideal i.e viscosity is zero.
- + Fluid is steady and continuous
- + Flow is incompressible.
- + Flow is rotational
- + Flow is along streamline, that is one dimensional

Shandappa
10/3/24
Course Coordinator
(Faculty in charge)

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Scheme of Valuation

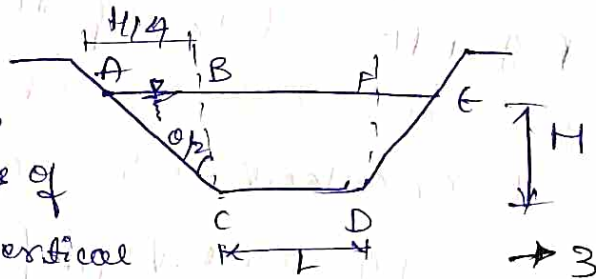
Bernoulli's Theorem: In a steady, ideal flow of an incompressible fluid, the total energy consists of pressure energy, kinetic energy and datum energy.

$$\frac{P}{\rho g} + \frac{V^2}{2g} + z = \text{constant.}$$

→ 1.5 7.5

3. a) Cipolletti notch:-

it is a trapezoidal weir, which has side slopes of 1 horizontal to 4 vertical



Thus in $\triangle ABC$

$$\tan \theta/2 = \frac{AB}{BC} = \frac{H/4}{H} = 1/4$$

$$\theta/2 = \tan^{-1}(1/4) = 14^\circ 2'$$

$$Q = \frac{2}{3} C_d (L - 0.2H) \sqrt{2g} H^{3/2}$$

→ 3

$$Q = \frac{8}{15} C_d \sqrt{2g} \tan \theta/2 H^{5/2}$$

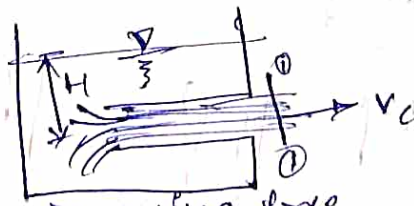
$$Q = \frac{2}{3} C_d L \sqrt{2g} \left[(L+ha)^{3/2} - ha^{3/2} \right] \quad \left[\because ha = \frac{V^2}{2g} \right]$$

→ 1.5 7.5

3. b) Borda's Mouthpiece Running free.



Running full



Running free.

→ (2)

Shardhanjali

Course Coordinator
(Faculty in charge)

Shardhanjali

Coordinator
(B.O.C)

Shardhanjali

Program Coordinator
(HOD CIVIL)



Scheme of Valuation

3.
b)

Total pressure = $\rho g a h$.

Rate of change of momentum = mass of fluid \times [final - initial velocity]
 $= \rho a_c v_c [v_c - 0] = \rho a_c v_c^2 \rightarrow (ii)$

$\rho g a H = \rho a_c v_c^2 \rightarrow (iii)$

$\rightarrow 3$

$$v_c = \sqrt{2gH}$$

$$\rho g a H = \rho a_c 2g \cdot H$$

Since there is no loss of head, $C_v = 1$

$$C_d = C_v \cdot C_c = 1 \times 0.5 = 0.5$$

$$Q = C_d a \sqrt{2gH}$$

$$Q = 0.5 a \sqrt{2gH}$$

$\rightarrow 2.5 \quad 7.5$

4
a)

Triangular notch

Given Angle of V-notch $\theta = 60^\circ$

Head over notch $H = 0.3m$, $C_d = 0.6 \rightarrow 2$

$$Q = \frac{8}{15} C_d \tan \frac{\theta}{2} \sqrt{2g} H^{5/2} = \frac{8}{15} \times 0.6 \times \tan \left(\frac{60}{2}\right) \times$$

$$Q = 0.53 \times 0.6 \times 0.57 \times 0.21$$

$$\left[\sqrt{2 \times 9.81} \times 0.3^{5/2} \right]$$

$$Q = 0.04 \text{ m}^3/\text{s}$$

$\rightarrow 2.5 \quad 7.5$

4
b)

Types of losses are Major losses

+ head loss due to friction

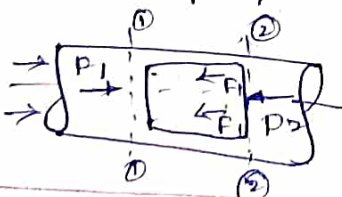
① Darcy Weisbach formula

② Chezy formula.

or minor losses

+ sudden expansion and contraction of pipe $\rightarrow 2$

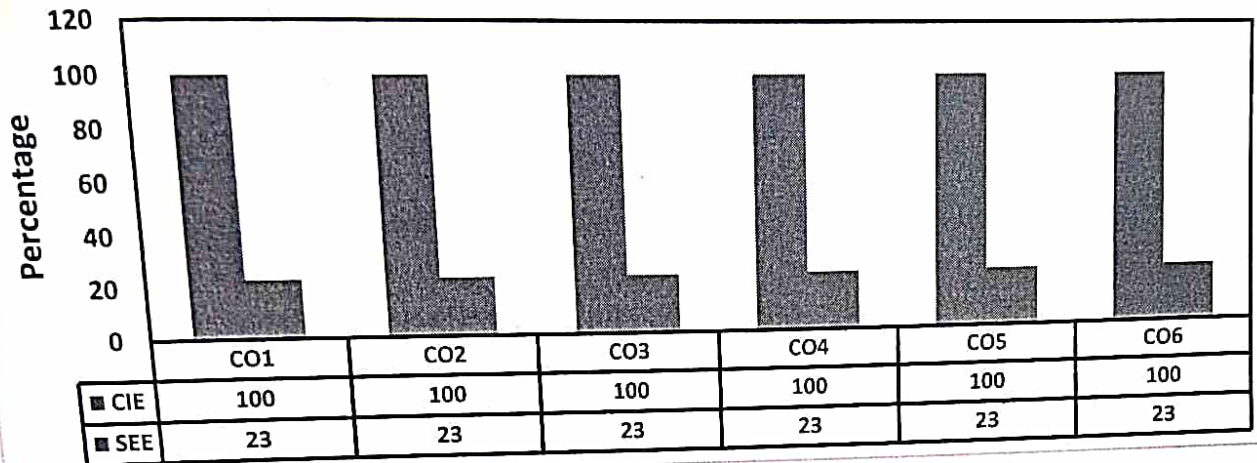
+ Bend in pipe & pipe fittings. $\rightarrow 3$



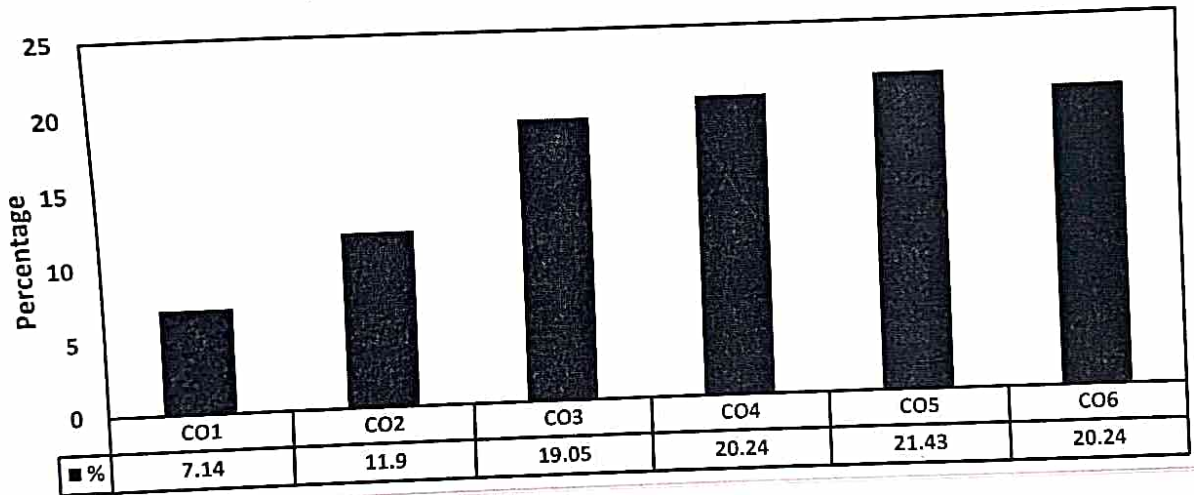
$$h_f = \frac{4fLV^2}{2gd}$$

$\rightarrow 2.5 \quad 7.5$

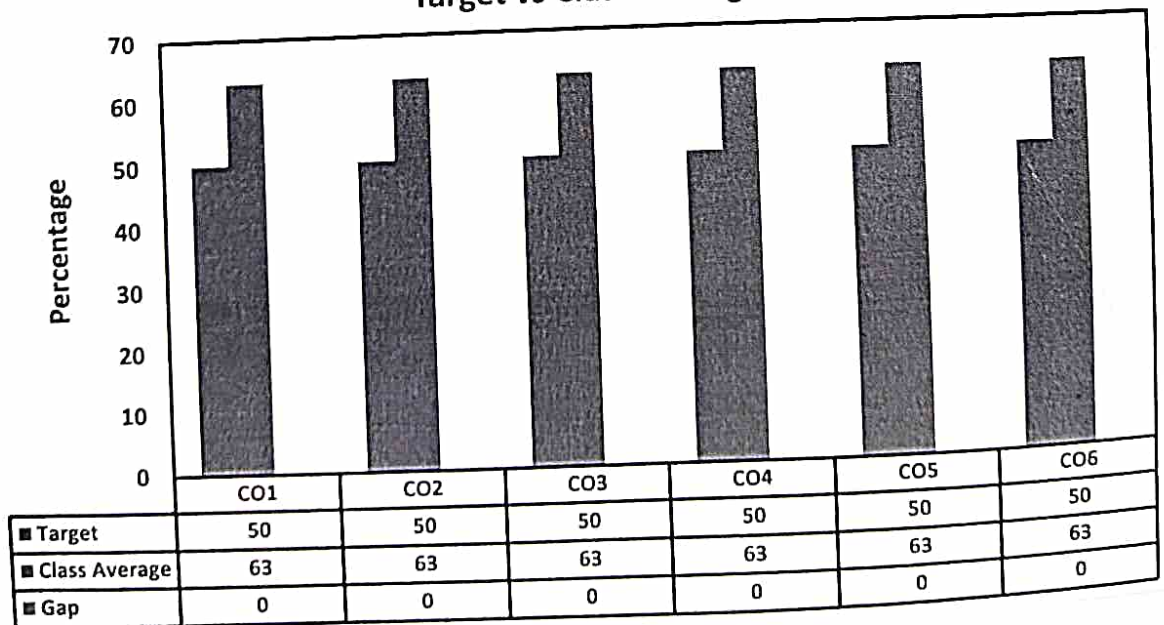
% of Students reaching more than the target



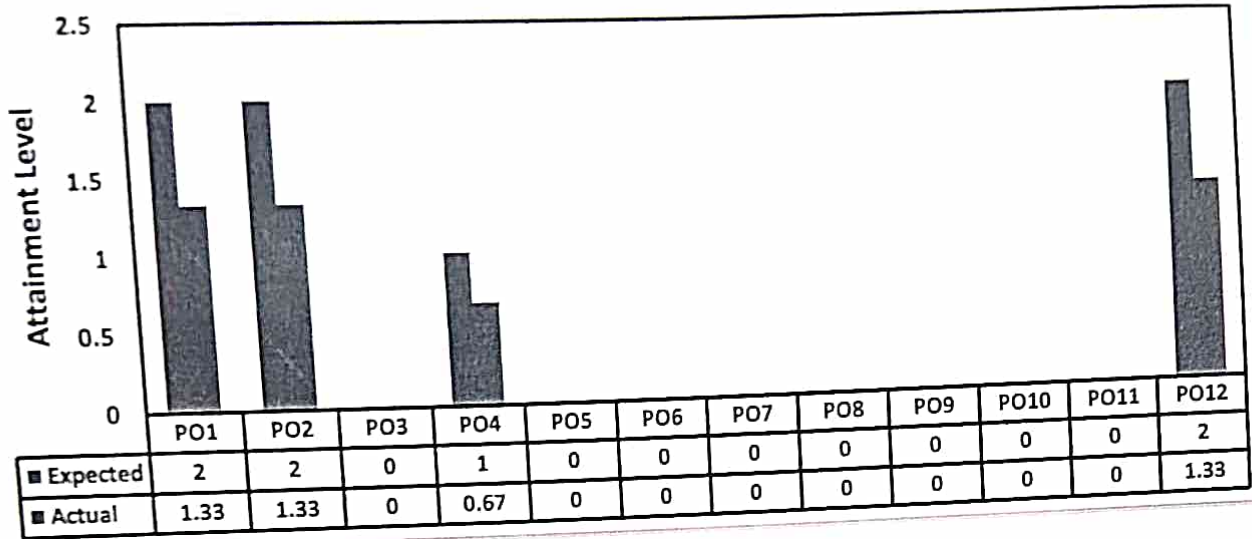
% CO marks distribution in CIE



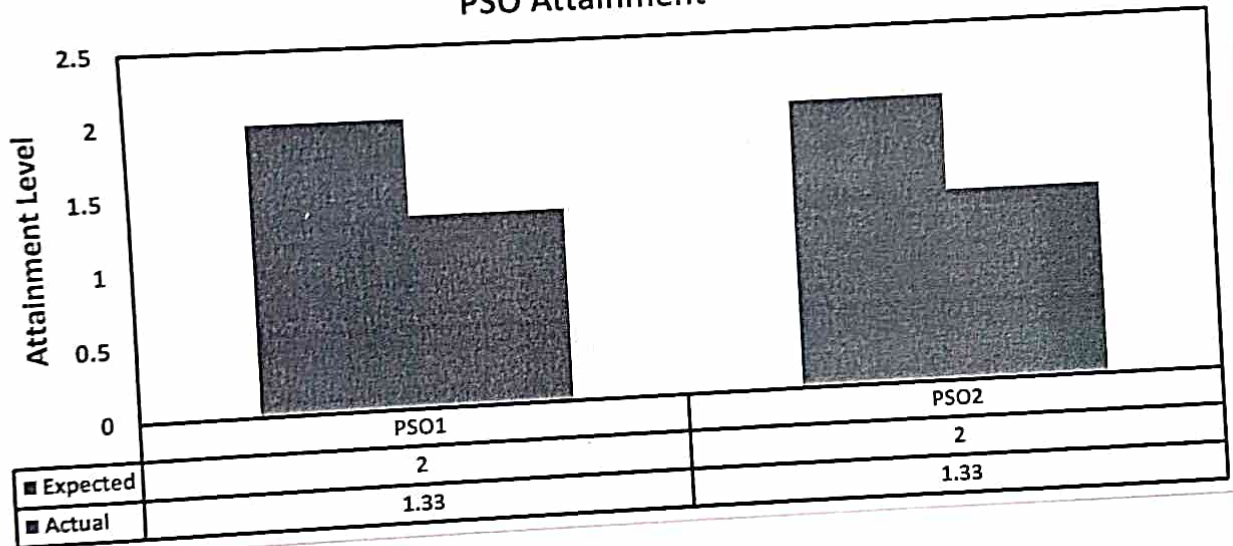
Target vs Class Average



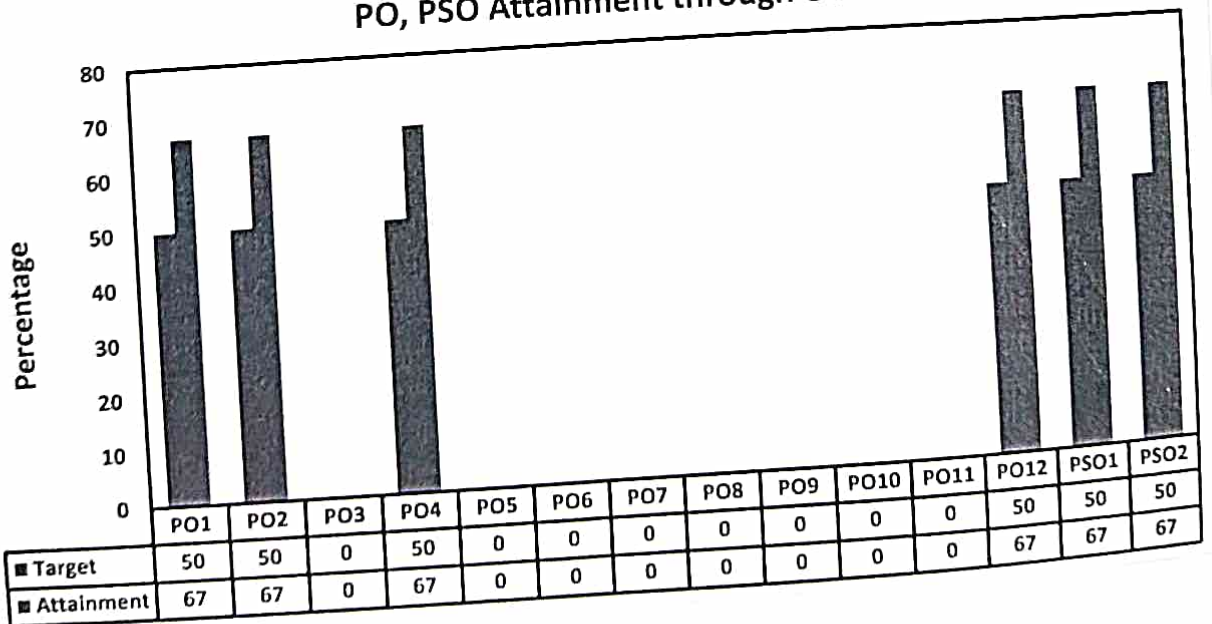
PO Attainment



PSO Attainment

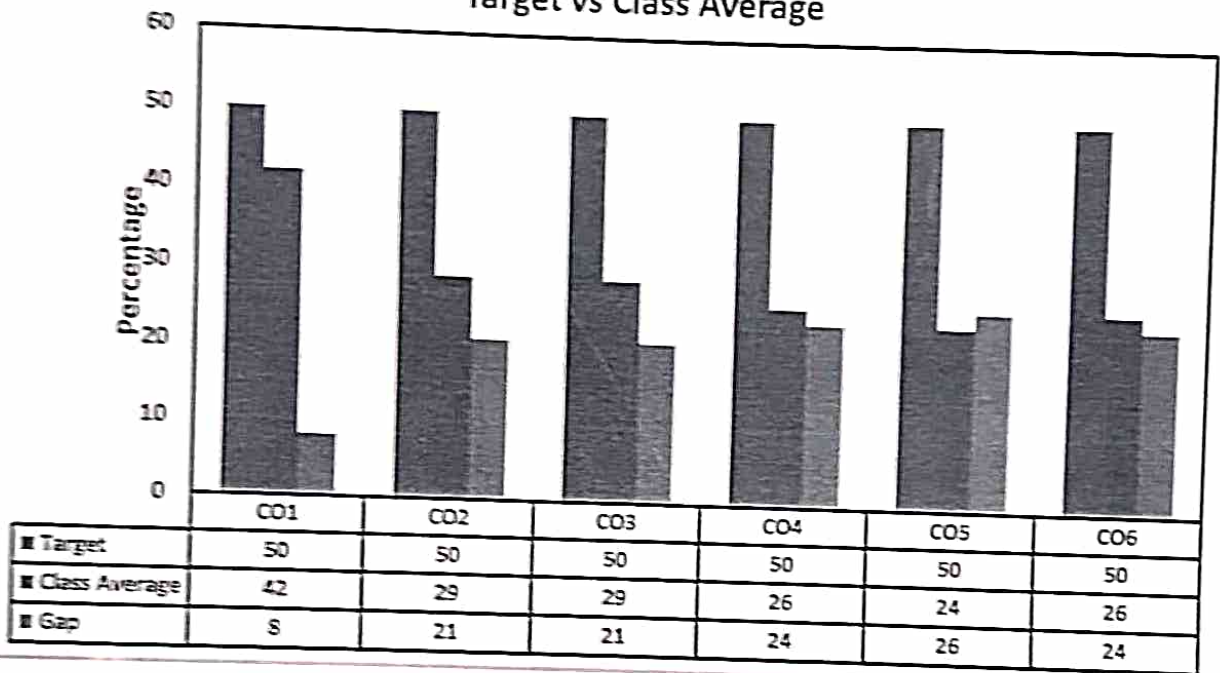


PO, PSO Attainment through COs

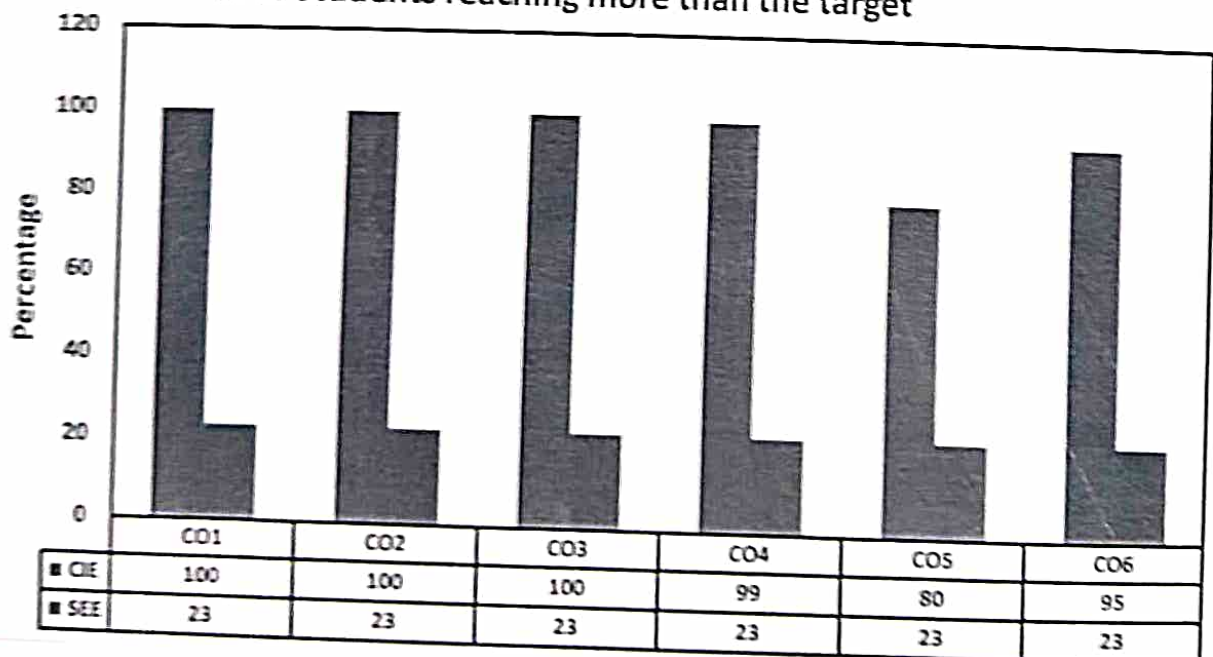


| | |
|------------------------|---------------------|
| Subject (Course) Title | Fluid Mechanics |
| Subject (Course) Code | 18CV33 |
| Semester | 3 |
| Section | A |
| Branch | CIVIL |
| Faculty incharge | Sri. SHARATHRAJ R M |
| Batch | 2018-2022 |
| Academic Year | 2020-2021 |

Target vs Class Average



% of Students reaching more than the target



1004

| | | | |
|---------------------|-----------------|---------------------|-----------|
| Department No. | 03 | Maximum Marks | 10 |
| Subject Title | FLUID MECHANICS | Course/Subject Code | 18CV33 |
| Semester | III A | Scheme | CBCS - 18 |
| Course Co-ordinator | Sharathraj R M | | |

Course Outcome Statements : After the successful completion of the course, the students will be able to

| | |
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Note : Answer all the questions.

| Q. No. | Question | Marks | RBT Level | CO |
|--------|---|-------|-----------|----|
| 1 | Derive an expression for discharge over Rectangular notch | 2.5 | L2 | 1 |
| 2 | Derive an expression for discharge over Trapezoidal notch | 2.5 | L2 | 2 |
| 3 | Explain with neat sketch Bord's mouth piece | 2.5 | L2 | 3 |
| 4 | Explain Hydraulic coefficients Cd, Cc and Cv | 2.5 | L2 | 3 |

| | | | |
|--------------------------|----|----|------|
| Last date for submission | 26 | 12 | 2020 |
|--------------------------|----|----|------|

| RBT (Revised Bloom's Taxonomy) Levels : Cognitive Domain | | |
|--|--------------------|---------------|
| L1 : Remembering | L2 : Understanding | L3 : Applying |
| L4 : Analysing | L5 : Evaluating | L6 : Creating |

Sharathraj R M
Course Coordinator
(Faculty in charge)

Sharathraj R M
Coordinator
DQAC

Sharathraj R M
19/12/2020
Program Coordinator
(HOD, Civil)



Result analysis information which is to be put in Course File

- a) Percentage CO covered / Percentage of CO addressed.
- Refer Graph Titled “% CO marks distribution in CIE” in Attainment Sheet.
- Note :** If you have written CO wise marks (from 3 CIE and Assignment) in Attainment sheet, you can get the above graph. If attainment is calculated considering final CIE and SEE marks, then get the graph from Excel sheet **which is attached herewith)**

b) CO-PO and CO-PSO Attainment

- Refer Graph Titled “PO Attainment” in Attainment Sheet
- Refer Graph Titled “PSO Attainment” in Attainment Sheet.

Note : You can also put graph titled “% of Students reaching more than the target” above the “PO Attainment” graph.

c) Percentage of students passed

| Branch | No. of students appeared for the exam | No. of students passed | Pass % |
|--------------------|---------------------------------------|------------------------|--------|
| Civil 3A
18CV33 | 68 | 48 | 71 |